ELECTRICAL POWER

DESIGN OF POWER TRANSFORMERS USING DIGITAL COMPUTERS'

A Thesis Submitted

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Ву



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SUMMARY

This thosis presents a design of power transformers for ratings from 500 K.V.A to 2000 K.V.A., medium voltages up to 22 kV, using digital computers.

By applying the theoretical study on the actual products present, a design for an 1000 K.V.A. transformer manufactured by EL NASH COMPANY FOR THE MANUFACTURE OF TRANSFORMERS AND ELECTRICAL PRODUCTS "ELMACO" in A.R.E., has been made, thus rendering the research more useful. Design particulars, such as customer requirements, operating conditions, standard specifications, iron lesses, copper lesses, reactance voltage drop, type of cooling, temperature limits, and short circuit duration for automatic circuit breaker choice, are taken into account.

The thesis includes introduction which gives a general description of power transformers and its basic elements (iron core, windings, tep-changer, cooling tubes, oil, expansion tank, dehydrating breather) and also gives a brief look at digital computers (operation, functional organization, Fortran language, Flow chart, ICL 1905E digital computer).

It contains historical review of important papers which had been done in the field of design of power transformers using ligital computers and general observations concerning these papers.

Previous work in programming for design of transformers of small ratings taking into account "Deng" paper by Oerliken Engineering Company in Switzerland together with modifications to suit local designs is included.

It also contains the means by which a program for the design of such transformers can be made, in such a way so as to give the necessary results with a large saving of effort and time. This program, prepared and executed using the "ICL 1905E" of the scientific computation center of Cairo University, has been applied to "KIMACO" transformers for ratings 500, 800, 1000, 1250, 1500 KVA, the latter being the maximum transformer rating manufactured by the Company.

Tables, containing output results of the above mentioned program for transformers up to 1500 KVA together with perfermance curves and technical comments, are included.

Extension of program possibilities for future developments in the manufacturing of locally produced power transformers of higher ratings are made. The program has been extended to include a rating of 2000 KVA. The program gives details of design and execution of one transformer in 26 seconds and for complete line production of Six transformers with different ratings, the required informations can be obtained in 41 seconds.

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List of Principal Symbols

The following are the symbols in general use throughout this thesis, unless otherwise stated, keeping in mind that the second symbol if found, referes to the digital computation work.

```
Qx
         = rated output in KVA
N
         = number of phases
\mathbf{F}
         = frequency in cycles/second
         = high voltage in volt/phase
Vl
V2
         = low voltage in volt/phase
Ur.URX
         = percentage resistance
Ux,Uxx
         = percentage reactance
Uk.UKX
         = percentage impedance
COSPH
         = power factor
SINPH
         = reactive power factor
VTl
         = starting volt/ turn.
V/T,VTX = final volt/turn
Q1
         = designed output in KVA
         = high tension current, amp.
Il
△1, CDIX = high tension current density, amp/mm²
\Delta2,CD2X = low tension current density.amp/mm<sup>2</sup>
Al, AClX = cross-sectional area of H.T. wdg., mm<sup>2</sup>
A2,AC2X = cross-sectional area of L.T.wdg. mm2
WLlX
         = height of copper cross-section of H.T.wdg..mm
BClX
         = breadth of copper cross-section of H.T.wdg.mm
```

```
Wlo.TLX
             = length of high tension winding before
                drying mm
TLR
             = length of high tension winding after
                drying , mm
m5, M5C
             = exact height of higher support of H.T.
                wdg., mm
             = length of low tension winding before
wlu.TLX2
                drying, mm
TLR2
             = length of low tension winding after
                drying . mm
             = exact height of higher support of L.T.
m3.M3C
                wdg. mm
             = maximum length of winding, mm
TIX,TIX1
who TBIX
                width of high tension winding . mm
whu,TB2X
                width of low tension winding, mm
DF'e
                effective diameter of core. mm
             = number of turns of high tension winding
N1.W1
                number of turns of low tension winding
N2.W2
Bl.BLX
                flux density in limb, gauss
By ,BYX
             = Flux density in yoke , gauss
                specific iron loss in limb, watt/kg
SLX
SYX
             = specific iron loss in yoke, watt/kg
io, IOX
             = percentage no load current
             = designed iron losses, watt
PD
             = area of limb, cm2
AL
             = area of yoke, cm2
Αу
                weight of limb, kg
Gl
```

4 4 1 h. sh. j

```
Gy
           ≥ veight of yoke. kg
P1(I)
           = guaranteed iron losses, watt
Dl
           = iner diameter of low tension winding.mm
D2
           = inner diameter of high tension winding, mm
Lml
           = mean length of high tension turn, m
Lm2
           = mean length of low tension turn, m
Gl
           = weight of copper of H.T.wdg., kg
G2
           = weight of copper of L.T.wdg, kg
Rl
           = resistance of high tension winding, ohm
Rl
           = resistance of high tension winding, ohm
R2
           = resistance of low tension winding.
Dm
           = mean diameter . mm
210
           = number of double coils
TS
              short circuit time
W1, W3, W5, W7, W9
           = corresponding number of high voltage turns
              at zero.
              +2.5,+5,-2.5,-5 percentage of tapping
V1, V3, V5, V7, V9
           = corresponding high voltages at zero.
              +2.5,+5,-2.5,-5 percentage of tapping.
Wll
           = number of turns with additional insulation
           = number of turns with normal insulation
W12
PCL
           = high tension copper losses, Watt
PC2
           ≥ low tension copper losses. Watt
PCT
           = total copper losses, Watt
PCT 75
           = total copper losses at 75°C . Watt
SOX1
           = factor for stray losses in percentage of
              PCT. Watt
PS
           = stray losses, Watt
```

= load losses , Watt PLPC (I) = guaranteed load losses, watt = surface area /total losses in H.T . Sixwdg..cm² /Watt. surface area / total losses in L.T. S2X wdg..cm²/ Watt temperature rise of copper in H.T.wdg.,C THAL PK1 temperature rise of copper in L.T.wdg.,C THAL PK2 mean temperature rise of oil, C TR temperature rise of oil at the tap.°C XMOT ZETAX1 factor for circulation height/length of winding = factor for cooling system height ETAXL losses/area for cooling system, Watt/m² GAMMAX1 permissible losses of tank, watt W.V PTI total designed losses, watt DELTAX = factor for maximum oil temperature TOM1 maximum temperature of oil upper limit, °C = height of cooling system, m HR HRX a AX2 = distance between top of tank and end of winding, mm XTN= number of tubes in one cooling system NCX number of cooling system = area of cooling system in horizontal FHdirection . m2 = area of cooling system in perpendicular F K direction . m2