

٢٠٢٤/٢

POWER FACTOR EVALUATION DURING TRANSIENT CONDITIONS IN CONVERTER-FED INDUCTION MOTORS

By

Hossny Hafez

HOSSAM EL-DIN MOHAMED GENDIA

B.Sc. (Eng.) 1980

X

A THESIS

Submitted in Partial Fulfilment

For the

DEGREE OF MASTER OF SCIENCE

in Elec. Engineering

To the

Electrical Power and Machines Department

AIN SHAMS UNIVERSITY

Supervised by

Prof. Dr. EL-SADEK A. KANDIL

Dr. AHMED D. EL-KOSHAIRY

1985



19125

EXAMINERS COMMITTEE

Prof. Dr. Abd El-Fatah Mahmoud Kheir El-Din
Professor at Fac. of Engineering,
Ain Shams University.

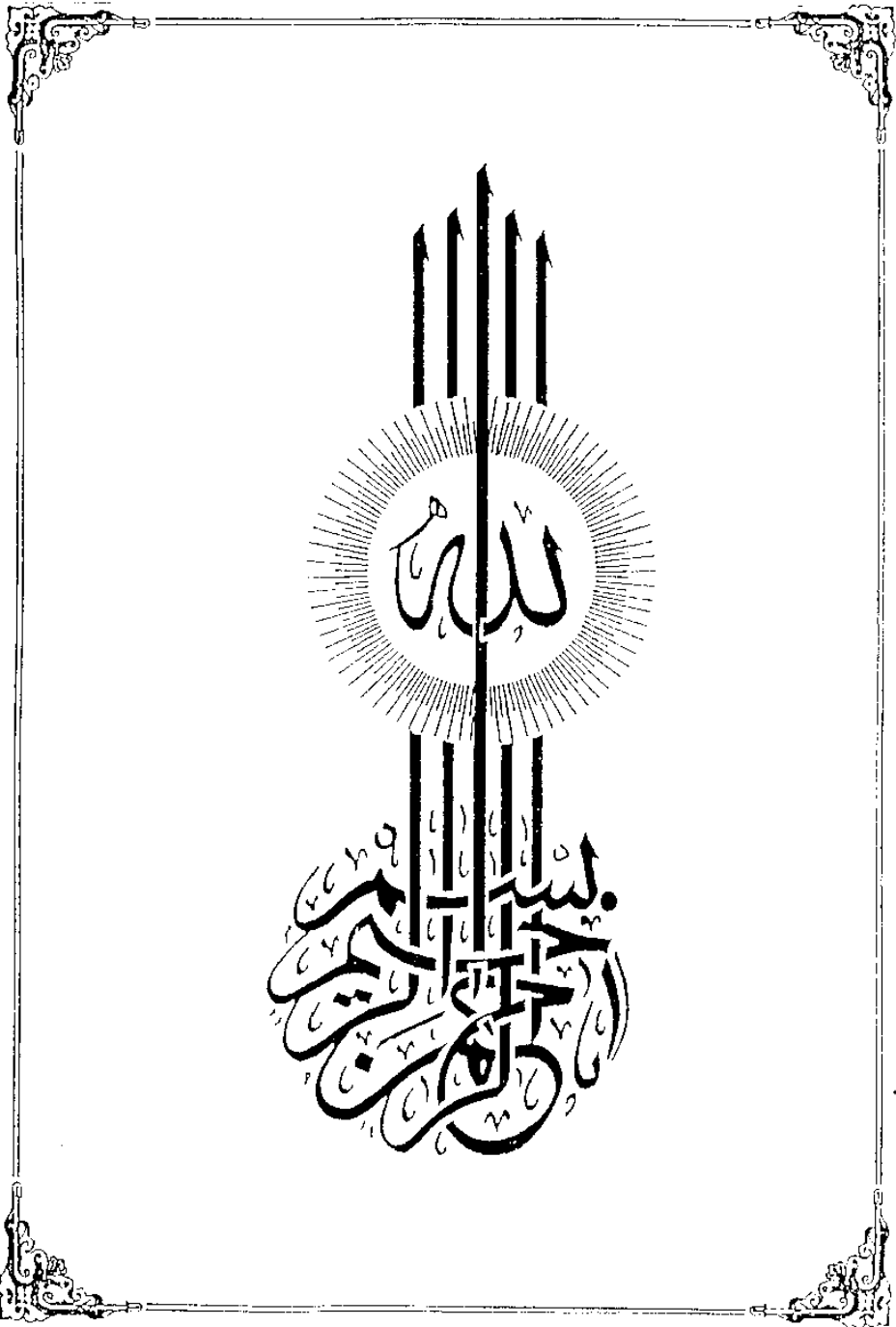
A. Kheir El-Din

Prof. Dr. Farouk Ismail Ahmad
Professor at Fac. of Engineering,
Cairo University.

F. Ismail

Prof. Dr. El-Sadek Amin Kandil
Professor at Fac. of Engineering,
Ain-Shams University.
(For the Supervisors).

El-Sadek Kandil



"In Name of Allah, the Compassionate, The Merciful"

To my beloved Late Mother,

and Dear Father,

I present my First Research Thesis

ACKNOWLEDGEMENTS

The author wishes to express his sincere gratitude to Prof. Dr. El-Sadek A. Kandil, head of Electrical Power and Machines Department at the University of Ain-Shams. He was my Professor, with the full meaning of the word. His teachings, inspiring guidance and continuous encouragement will be ever remembered with great gratitude.

The author is also greatly grateful to Dr. A. Deyaa El-Koshairy for suggesting the topic of the research, continuous supervision and valuable discussions during the course of this thesis. His help and patience, particularly during the computer programming period, and the experimental work, are highly appreciated.

Thanks are also due to Dr. M.A. Badr, Prof. and Supervisor of the Electrical Machines Laboratory at the University of Ain-Shams, for his kind help and guidance in the experimental part of the research.

TABLE OF CONTENTS

	Page
SUMMARY	i
NOMENCLATURE	iv
ABSTRACT	vi
1. INTRODUCTION	1
2. FORMULATION OF THE PROBLEM.	10
2.1 Voltage and Current Relations	12
2.2 Transformations to d-q Axes Variables . . .	16
2.3 Basic Machine Relations in d-q Axes Variables	18
2.4 Voltage Equations for Specific Reference Frames	21
2.5 Torque Equation	24
2.6 Power Factor Equation	24
3. SOFTWARE DESCRIPTION.	27
3.1 Introduction	27
3.2 Transition-Matrix Method	29
3.3 Runge-Kutta Method Modified by Gill	32
3.3.1 Description of Gill method	35
3.3.2 Order of the calculation	35
3.4 Sampling Theorem	38
4. THEORETICAL RESULTS.	42

	Page
5. EXPERIMENTAL WORK.	76
5.1 Description	76
5.1.1 The torque Measuring unit	76
5.1.2 The generalised machine	81
5.1.3 Oscilloscope	88
5.1.4 Tacho-generator	89
5.1.5 Low-pass filter	90
5.1.6 Visicorder	92
5.2 Parameters of Motor Under Test	93
5.3 Experimental Results	94
CONCLUSIONS.	110
REFERENCES.	112

S U M M A R Y

Power factor is of big concern to electricity utilities for well known reasons. The problem of power factor evaluation of induction motors when operated under variable speed conditions, has not been considered yet.

Two cases of supply voltages are handled, these are; constant frequency constant voltage and variable frequency variable voltage sources, keeping motor flux virtually constant.

Conventional power and power factor meters can not trace the fast and continually varying electrical quantities, under transient conditions owing to their limited frequency range and slow speed of response. The problem becomes more severe when the motor is supplied from a variable frequency voltage converter due to presence of distorted current and voltage waveforms.

A recent trend has been to use static transducers to calculate power from the voltage and current signals.

This thesis presents a method by which a complete transient analysis is made for the motor and its connected mechanical load during a specified load duty cycle. The voltage and current waveforms are plotted versus time for the whole load cycle. A good estimation for the power factor is made by detecting the points of positive going zero crossing on the voltage and current waveforms. The cosine of the resulting phase angle displacement at each cycle against time represents the transient displacement factor pattern which repeats itself upon the completion of each load cycle. An effective power factor can be calculated for the drive, from the obtained pattern which depends on the nature of the mechanical load.

Since the set of differential equations of the induction motor and its mechanical load, are nonlinear when motor speed varies substantially, a numerical method is needed.

The theoretical results are obtained using two methods; transition matrix method and Runge-Kutta method modified by Gill. Both methods gave the same results. However, most of the calculations are made by the first method since it uses relatively smaller computing time.

The researcher persued the experimental work to confirm the effectiveness of the theoretical results. Transient currents, voltages, speed and torque are recorded during motor acceleration under load and no load conditions. A torductor manufactured by ASEA is used to trace motor torque. A dual-channel oscilloscope is used to record two variables at a time. To extend the time base for the current and voltage waveforms for easy comparison with the theoretical results, a visicorder manufactured by HONEYWELL is used for this purpose. Theoretical and experimental results showed good agreement.

The method presented here to evaluate the overall power factor during speed variations, though simple proved very effective. A microcomputer and knowledge on motor data and load duty cycle are enough to evaluate the effective value of power factor. Also, the thesis shows that motor overall power factor is much better when operated from a variable frequency voltage source rather than from a constant frequency voltage source, as far as variable speed operation is concerned.

NOMENCLATURE

1, 2	suffixes denoting stator and rotor, respectively.
d, q	suffixes denoting axes rotating synchronously with supply frequency.
λ	instantaneous flux linkage.
p	differential operator, d/dt
P	number of poles.
m	number of phases
r	resistance
t	superscript denoting transpose of matrix
a, b, c	phase quantities in stator windings
A, B, C	phase quantities in rotor windings
i	instantaneous current
v	instantaneous voltage
θ	electrical angle denoting instantaneous rotor position, radians
w	angular frequency of supply voltage, rad/s.
T	iteration interval, seconds
L_{11}, L_{22}	self-inductances of three-phase stator and rotor circuits, respectively.
L_{ab}, L_{bc}, L_{ac}	mutual inductance between stator phases.

1/

v

L_{AB}, L_{BC}, L_{AC}	mutual inductance between rotor phases.
L_{12}	mutual inductance between three-phase stator and rotor circuits.
T_L	external load torque.
J	inertia of motor and connected load.
D	coefficient of friction.
ω_r	mechanical speed, rad/s.

ABSTRACT

The problem of evaluating an effective value for the power factor of an induction motor driving a load with known load duty cycle is not solved yet. Examples of such loads are motors operated from conventional ac supply with frequent starting and stopping loads such as lifts and hoists also, inverter fed induction motors driving variable speed loads such as printing machines and machine tools. Several large thyristor installations are now in operation throughout the world, without paying operational penalties due to poor plant power factor. Induction motors operating under these conditions may cause very poor effective power factor at the power lines feeding them. Unfortunately electric measuring devices would not respond to fast changes in voltages and currents and their high order harmonics due to device limited frequency range. The thesis presents a scheme by which varying transient power factor can be calculated for variable speed induction motor drive as function of time. The resulting power factor pattern can be used to define an effective power factor according to which a new tariff system can be implemented

to take into account the hidden reduction in power factor for such induction motor operating conditions. Two cases are treated in this paper, namely, motors using direct switching to conventional ac supply and motors fed from variable frequency inverters. The Transition-Matrix method is used to numerically solve the non-linear differential equations of the motor and its connected mechanical load.

CHAPTER (1)

INTRODUCTION

Primarily, induction motors have been considered as constant speed drives, and the great majority of their applications depend on constant supply frequency. The advent of high-current transistors and silicon controlled rectifiers and their use in inverters and cycloconverters has ended the limitations of an induction machine for constant speed service and a new era started for the induction motors for controlled variable speed applications. Then, by using solid-state frequency changers to supply power to induction machines is now finding applications in many areas, which previously had been the private domain of the d.c. machine. The ease of designing modern controlled semi-conductors devices and their reliability made it useful in inverters and cycloconverters which have resulted in the constantly increasing applications of induction machines in variable speed drive systems. Starting conditions of an electric drive in a composite load is a process of transition of the motor and the associated mechanical load. Starting of motors forms an important part of their operating conditions. When designing an electric drive and choosing the corresponding