

AIN SHAMS UNIVERSITY
FACULTY OF ENGINEERING
DEPT. OF ENERGY & AUTOMOTIVE ENGINEERING



PLATES TORQUE DECAY OF MULTIPLATE

FRICITION CLUTCH

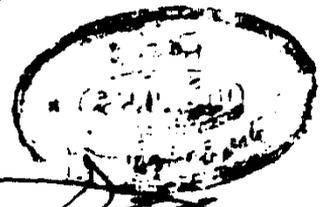
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This is submitted for the partial fulfilment
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by

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CONTENTS

Page

ACKNOWLEDGMENTS

SUMMARY -----	1
NOTATIONS -----	11
INTRODUCTION -----	1

CHAPTER ONE :

FACTORS AFFECTING THE SERVICE - LIFE

OF FRICTION CLUTCHES-----	1
1.1 Function of Friction Clutches -----	4
1.2 Design Factors -----	5
1.2-1 Coefficient Of Friction -----	7
1.2-2 Spline Friction -----	10
1.2-3 Plate Width -----	16
1.3 Service-Life Factors -----	19
1.3-1 wear -----	19
1.3-2 Driver -----	23
1.3-3 Maintenance -----	25

CHAPTER TWO :

RELIABILITY FUNCTION OF THE

MULTIPLATE PACK -----	27
2.1 Reliability Function of a Pair of	
Friction Surfaces -----	27
2.2 Torque Decay shape Functions	
of The Pair of Friction Surfaces -----	31
2.2-1 The Straight line Shape Function -----	34
2.2-2 The Parabolic Shape Function -----	35
2.2-3 The Exponential Shape Function -----	36
2.2-4 The Ideal Shape Function -----	37
2.2-5 Evaluation of Shape Functions -----	37

3.2-1 Reliability of Partially Parallel System with Initially Different and Time Dependent Failure Rates For Its Elements	51
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CHAPTER THREE :

PRACTICAL ESTIMATION OF THE RELIABILITY FOR THE MULTIPLATE PACK	44
3.1 Introductory Survey	44
3.2 Distribution Function of Multiplate Pack Failure	45
3.2-1 Application	47
3.3 Estimation Of Failure of Pair of Friction Surfaces	53
3.4 Determination of Number of Cycles Per Kilometer	58

CHAPTER FOUR :

PLATES TORQUE DECAY OF THE MAIN CLUTCH OF A HEAVY VEHICLE	59
4.1 Reliability Calculation of individual Pairs of Friction Surfaces	59
4.2 Reliability Calculation of The Multiplate Pack	69
4.3 Analysis of Results	73
4.3-1 General	73
4.3-2 Assumptions Made	76
4.3-3 Analysis of Pairs of Friction Surfaces Failure Mode	77
4.3-4 Analysis of Multi-Plate Pack Failure Mode	78

APPENDIX 2

CONTENTS

5.1 Field Failure Data -----	101
5.2 Torque Decay Shape Functions -----	102
5.3 Future Work -----	103

CONCLUSION

The torque capacity of friction clutch decreases during its service-life down to a value at which the clutch fails to transmit the applied torque.

The reliability of the clutch can be improved from the knowledge of the torque decay function i.e reducing the number of clutch failures.

The prediction of the torque decay shape function for the elements of the multiplate clutch pack is achieved by the help of the reliability theory and the field failure data.

To arrive at the torque decay shape function theoretically, three shape functions (parabolic ,straight line and exponential shape functions) have been tried.

A field study is done on a multiplate friction clutch of a heavy vehicle to obtain the distribution function of covered kilometers by the vehicle to the failure of the clutch . The comparison of the practical and the theoretical results which are based on the three shape functions, shows that the suitable torque decay shape function is a compound function . This function composes of a straight line to about 70% of the service-life of the clutch plate, and parabolic function to the end of life .

This compound function gives results in acceptance with the practical results at confidence level of 99% .

NOTATIONS

- A Effective area of a friction surface.
- A_j Friction work done during the j^{th} cycle.
- a Ratio of internal and external radii of a friction surface.
- B Constant.
- $C_1^{(ns)}$ Combination of 1 out of ns .
- $\bar{t}(\cdot)$ Expected value (arithmetic mean).
- $F(j)$ Difference between summation of hazard functions when there are j failures in the system.
- F Friction force.
- $f(x)$ Probability density function of the stress.
- G Geometry factor .
- $g(Y)$ Probability density function of the strength.
- $h_j(\cdot)$ Hazard function of the j^{th} element.
- h_j^n Hazard function of the j^{th} element when there are n failures in the system .
- I_1 Rotating inertia belongs to a power unit.
- I_2 Rotating inertia belongs to a working unit.
- KE Covered kilometers to joint point of straight line shape function and parabolic one.
- K Coefficient of proportionality.
- k Covered kilometers .
- k_f Covered kilometers to failure.
- k_i Covered kilometers to failure of the i^{th} vehicle.
- k'' Proportionality factor.
- l Real numbers 1,2,3 and 4 .

- σ Standard variate.
- n_1 Total number of tested vehicles in 10 hours -
 tested sample.
- α_j Fraction of probabilities with indices j .
 j indicates the number of failed elements and j
 the index of elements in the system.
- β_0 Mean number of occurrences per unit time.
- β, β_1 Dynamic factor considering and neglecting
 spline friction.
- β_2 Shape parameter of Weibull distribution.
- γ Location parameter of Weibull distribution.
- γ_1 Coefficient shows how the 1- shape function
 is near to the ideal case.
- η Scale parameter of Weibull distribution.
- θ Value corresponds to number of occurrences.
- θ_1 Mean angle between normal force on tooth of
 rotor plate and tangent to circumference.
- θ_2 Mean angle between normal force on tooth of
 stator plate and tangent to circumference.
- $\omega_N(t)$ Probability of N occurrences in 0 to t time.
- μ_1 Coefficient of friction between plates.
- μ_2 Coefficient of friction between rotor plate
 and splines.
- μ_3 Coefficient of friction between stator plate
 and splines.
- $\sigma_{..}$ Square root deviation of..
- σ_1 Square root deviation of the torque capacity
 of the pair of friction surfaces.
- σ_2 Square root deviation of the applied torque
 on the pair of friction surfaces.

INTRODUCTION 1

The torque capacity of friction clutch decreases during its service - life down to a value at which the clutch is unable to transmit the applied torque. In this case the clutch is said to be failed.

Determination of the form of the torque decay shape function helps to improve the clutch reliability (reduce the number of failures).

The prediction of the torque decay shape function of the elements of the multiplate pack of the clutch enables the designer to have the reliability equation as a function of design parameters. Then a parametric study can be made for minimization of the number of failures .

The design parameters are the coefficient of friction between plates, the coefficient of friction between the plates and splines, compressive force on plates, number of plates , dynamic factor , and dimensions of the plates.

This work concentrates on the prediction of the torque decay shape function for the elements of the multiplate clutch pack .

This is achieved by the help of reliability theory and field failure data .

Fig.(1) shows the method of fulfilment the task .

c1

Reliability is the probability that a system can perform its function correctly in a given period of time under the given operating conditions. Reliability evaluation is derived by practical or theoretical means. Practical evaluation needs special techniques of testing, to process the data collected, and to interpret the information in a meaningful fashion, or to collect appropriate data from field of experience. Theoretical evaluation of reliability needs to formulate a reliability mathematical model which is an adequate representation of the component (aggregate) being considered. Thus involving the techniques of probability theory, mathematical modelling and various specialized mathematical concepts.

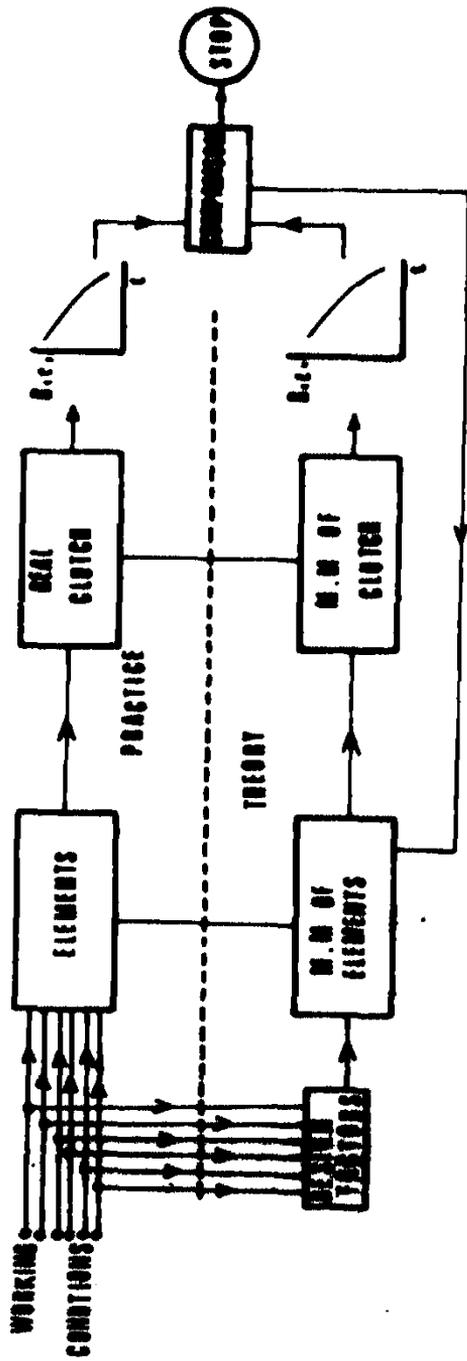


FIG.(1) PROCEDURE OF ESTIMATION OF PLAIT TORQUE DECAY

$R(t)$ Reliability function of time t

M.N..... Mathematical model

CHAPTER ONE : FACTORS AFFECTING SERVICE-LIFE OF
FRICION CLUTCHES :

The friction clutch Fig.(1.1) consists of driving parts, driven parts and release mechanism . It is better to study the function of the friction clutch before dealing with the factors affecting the service-life.

1.1 Function of Friction Clutches [1]^{*} :

The clutch transmits power from a power source to a stationary or moving component until the two are moving at the same speed, that is ; until there is no relative angular velocity between driving and driven parts. Consider two rotating inertias I_1 and I_2 rotate with unequal angular velocities ω_1 and ω_2 at time t_0 and ω_1 and ω_2 at any instant. Let I_1 belongs to a power source giving a torque M_d and I_2 belongs to a working unit having a resisting load torque T_2^+ . Furthermore, let the clutch transmits a torque T .

The function of the clutch-according to Fig. (1.2)- is as follows :

- (1) Let the engagement of the clutch starts at time $t = 0$, the clutch torque T increases up to

* Number of reference

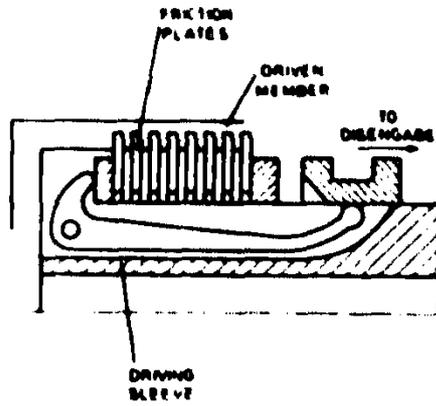


Fig.1.1 Design of multi-plate clutch [6]

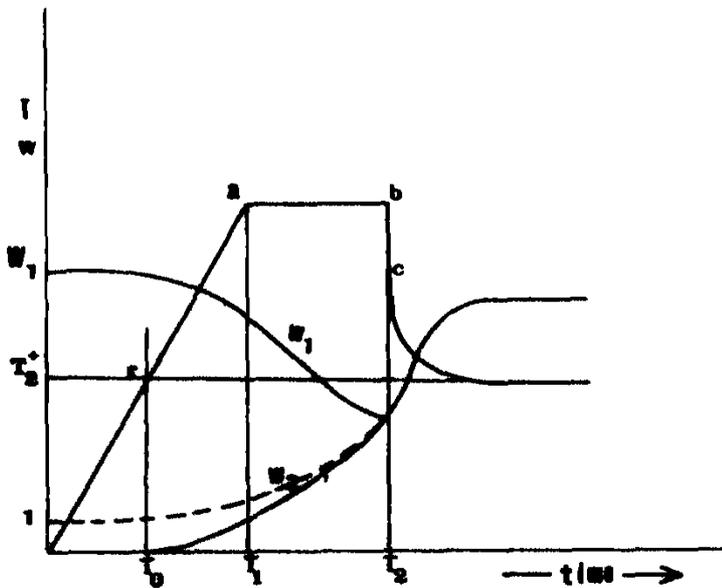


Fig.1.2. Function of the clutch

the value of the resisting torque T_2^+ at the point r. The driven parts begin to move at time t_0 .

- (2) After full engaging the clutch torque becomes maximum (point a). The angular velocity of driven parts increases during the time $(t_0 - t_1)$.
- (3) During the time t_1 to t_2 , even the clutch is fully engaged, it goes on slipping. The value of w_2 increases and the value of w_1 decreases. The torque T is constant during this period.
- (4) At time t_2 , the clutch will rotate as one solid body ($w_1 = w_2$).
- (5) For vehicles, if M_d is the torque of the engine, and T_2^+ is the resisting torque transferred to driven shaft of the clutch, the diagram represents the starting of the motion of the vehicle.
- (6) If the angular velocity of the driven parts of the clutch varies from zero (point 1), then the diagram shows the shift to higher gear.

1.2 Design Factors :

It is meant by the design factor that one defined by the designer as dimensions, number of plates $(n+1)$, coefficient of friction between surfaces μ compressive force P and dynamic factor β . The relations between some parameters will be studied.