AIN SHAMS UNIVERSITY **FACULTY OF ENGINEERING** CIVIL ENGINEERING - IRRIGATION AND HYDRAULICS

Ph.D. THESI

GROUND WATER QUALITY MODEL WITH DECAYING POLLUTANTS

BY

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This dissertation is submitted to Ain Shams University for the degree of Philosophy Doctor in Civil Engineering.

The work included in this thesis was carried out by the author in the Department of Irrigation and Hydraulics, Ain Shams University, from September 1989 to September 1993

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Abstract:

Groundwater constitutes an important component of many water resource system, supplying for domestic use, for industry, and for agriculture. Therefore, groundwater must be managed carefully to be the most beneficial use. Good management requires the ability to forecast the aquifer's response to planned operations, such as pumping and recharging. The response may take the form of changes in water levels, changes in water quality, or land subsidence. Any planning measures to consider mitigation, clean-up operations, once contamination has been detected in the saturated or unsaturated zones, requires the prediction of the path and the fate of the contaminants in response to the planned activities. For most practical problems, because of the heterogeneity of the considered domain, the irregular shape of its boundaries, and the nonanalytic form of various source functions, only a numerical model can provide the required forecasts. In this work, a numerical model has been developed to simulate the groundwater flow and conservative and nonconservative pollutant transport through the saturated porous media. The Finite Element Method has been used to solve the partial differential equations that govern the groundwater flow and solute transport. Problems with available analytical or numerical solutions have been used in order to verify the capability of the model in simulating the different field situations in one- or two- or three-dimensions. The model has been applied to a selected region in the East Nile Delta in Egypt in order to calibrate the aquifer properties. Also the has been applied to hypothetical three-dimensional problems which may be occurred in the real world. can be used efficiently concluded that the model simulating and predicting the successfully in conservative and nonconservative pollutants in aquifers under a variety of conditions with the minimum of simplifying assumptions.

NOTATION

a	Compressibility of water	$[LT^2M^{-1}]$
A _{ij}	Conductance matrix	$[L^2T^{-1}]$
A _e	Elemental area	[L ²]
$\mathtt{a}_\mathtt{T}$	Transversal dispersivity	[L]
$\mathtt{a}_\mathtt{L}$	Longitudinal dispersivity	[L]
$\mathbf{a}_{\mathbf{v}}$	Vertical dispersivity	[L]
B _{ij}	Storage matrix	[L ²]
b	Compressibility of the aquifer	$[LT^2M^{-1}]$
b'	Thickness of the layer that represents the stream	ı
	bottom.	[L]
С	Concentration of the solute	$[ML^{-3}]$
Cn	Courant number	
C "	Ratio between the mass held on the solid surface a	and the
	mass of the solids in solution	
Cin	Concentration of the inflowing water in the case of	£
	infiltration or the average concentration in the a	aquifer
	in the case of abstraction of water	[ML-3]
ď,	Effective grain diameter	[L]
di	Thickness of the aquitard	[L]
D'i	j Hydrodynamic dispersion-diffusion coefficient	$[L^2T^{-1}]$
D_{md}	Molecular diffusion coefficient	$[L^2T^{-1}]$
Do	Diffusion coefficient in a free water system	$[L^2T^{-1}]$
	At Time step size	[T]
Δ	Elemental cross-sectional area of cubic element	
	perpendicular to the pore-water velocity	$[L^2]$

Element number erfc(x) Complementary error function= 1- erf(x); IL^21 Gii Capacitance matrix $[LT^{-2}]$ g Gravity acceleration [L] h Hydraulic head $[L^2]$ k Permeability [LT-1] Kij Hydraulic conductivity tensor [LT⁻¹] K_{vi} Vertical hydraulic conductivity of the aquitard L^3M^{-1} Ka Distribution coefficient Hydraulic conductivity of the layer that represents the k' $[LT^{-1}]$ stream bottom $[MT^{-1}]$ J_{disp.} Dispersive flux $[T^{-1}]$ l, Aquitard resistance i T^{-1} λ Decay constant [L] Aquifer thickness N. Total number of elements. $[ML^{-1}T^{-1}]$ μ Viscosity n_e Effective Porosity NP Total number of the nodal points $N_{i}(x, y)$ Shape function. $\int L^2 T^{-1}$ Kinematic viscosity $\partial h/\partial x_i$ Hydraulic gradient in the j-direction; $[ML^{-4}]$ $\partial C/\partial x_i$ Concentration gradient in the direction i P, Peclet number $[L^2T^{-1}]$ Pij Solut tran. conductance matrix L3T-1 tQ; Sink or source flow rate at the node i Concentration of the solute of a source or sink of a OC' $[ML^{-3}T^{-1}]$ strength which is assumed to be known

q_{i}	Average discharge in the direction i	[L3T-1L-2
T _{liquid} Water filled area perpendicular to the direction of		
	Darcy's velocity	[L2]
Re	Reynold's number	
ρ	Density of water	[ML-3]
R	Retardation factor.	
r	Distance from the pumped well	[L]
ρ_b	Bulk density of the porous media	[ML ⁻³]
Pary	, Dry matrix material	[ML ⁻³]
S	Storativity of the aquifer	
s _o	Specific storativity)	[L-1]
T	Transmissivity of the aquifer	$[L^2T^{-1}]$
t	Time	[T]
t.5	Half-life of the isotop	[T]
V	Velocity resultant	[LT ⁻¹]
V_{b}	Elemental bulk volume	[L3]
v_{e}	is the volume of the element	[L ³]
W(u,r/B) Hantush well function		
∇	vectorial-delta $(\partial/\partial x + \partial/\partial y + \partial/\partial z)$	[L-1]
!	the factorial	

au Time factor

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