Ain Shams University

Faculty of Engineering

Irrigation and Hydraulics Department

Design of Stilling Basins Using Artificial Roughness

A Thesis Submitted in Partial Fulfilment of the Master Degree Civil Engineering – Irrigation and Hydraulics department

By

Shaimaa Fathy Aly Ebrahim Younis

B.Sc. Civil Eng.—Ain Shams University

Supervised by

Prof.Dr. Nahla Mohamed AboulAtta

Professor of irrigation design
Irrigation and Hydraulics Department
Faculty of Engineering- Ain Shams University

Dr. Ghadah. M. Samy Azizah

Assistant professor
Irrigation and Hydraulics Department
Faculty of Engineering- Ain Shams University

Dr. Nevin Yousif Saad

Lecturer

Irrigation and Hydraulics Department
Faculty of Engineering- Ain Shams University

Table of Content

Abstract	XII
Chapter 1 INTRODUCTION	1
1.1 Scope of Work	2
1.2 Objectives	2
1.3 Plan of Study:	
Chapter 2 LITERATURE REVIEW	
2.1 Hydraulic Jump on Smooth Horizontal Floors:	5
2.2 Effect of Stilling Basins on the Flow:	
2.2.1 General considerations for design the stilling basin:	
2.2.2 Some types of stilling basin according to the United States Bu	
Reclamation (USBR):	
2.2.3 Stilling basins with blocks:	
2.2.4 Stilling basin with roughness:	
Chapter 3 THEORETICAL APPROACH	19
3.1 The Dimensional Analysis:	20
3.2 The Macroscopic Approach:	
3.2.1 The relative sequent depth Y2/Y1:	24
3.2.2 The relative energy loss, E_L/E_1 :	27
Chapter 4 EXPERIMENTAL WORK	29
4.1 The Hydraulic Equipments	29
4.1.1 The flume	
4.1.2 The sluice gate	32
4.1.3 The tail gate	
4.2 Measuring Devices:	
4.2.1 Discharge:	34
4.2.2 Water surface configurations measurement:	
4.2.3 Measurement of longitudinal distances:	36
4.3 Bed Roughness:	36
4.4 The Experimental Plan:	42
4.4.1 Determination of the best intensity:	
4.4.2 Determination of the best roughness length:	42
4.4.3 Comparison between the T-shape roughened stilling basin and	
rectangular shape stilling basin	
4.5 Test Procedure:	
4.6 Test Results: (Appendix A)	
Chapter 5	45
ANALYSIS AND DISCUSSION OF EXPERIMENTAL WORK	45
5.1 The Effect of Roughness Intensity on Flow Characteristics:	45

5.1.1Water surface configuration for different intensities and constan	
roughness length:	5
5.1.2 The relative length of jump (L_j/Y_1) for different intensities and and	_
constant roughness length: 4	J
5.1.3 The relative sequent depth of the hydraulic jump for different	
intenisties and constant roughness length ($\frac{Y_2}{Y_1}$):	4
5.1.4 The relative energy loss (E_L/E_1) :	
5.2 The Effect of Roughness Length on Flow Characteristics:	5
5.2.1 Water surface configuration for different jump lengths and constant	
intensity:65	5
5.2.2 The Relative Length of Jump $(\frac{L_j}{Y_1})$ for different jump lengths and	
constant intensity:	
5.2.3 The relative jump sequent depth (Y_2/Y_1) for different jump lengths	
and constant intensity:	3
5.2.4 The Relative energy loss (E_L/E_1) for different jump lengths and	
constant intensity:	
5.3 Comparison Between T-Shape and Rectangular Shape of Roughness 80	
5.3.1 Economical point of view:	
5.3.2 Efficiency point of view: 8.	
5.4 Studying the Efficiency of Stilling Basin Using T-shape Roughness: 86	
5.5 The Sensitivity Analysis:	3
Chapter 6 CONCLUSIONS AND RECOMMENDATIONS	J
6.1 Conclusions: 90	0
6.2 Recommendations: 92	2
References 92	3
APPENDIX A	7
APPENDIX B	5
ARABIC SUMMARY 13	1

List of Symbols

Symbols	Refers to	Dimensions	Units
a,b	Coefficients of relative jump length depend on intensity	$M^0L^0T^0$	unitless
a`,b`	Coefficients of relative sequent depth depend on intensity	$M^0L^0T^0$	unitless
a``,b``	Coefficients of relative energy loss depend on intensity	$M^0L^0T^0$	unitless
c, d	Coefficients of relative jump length depend on relative roughness length	$\mathrm{M}^0\mathrm{L}^0\mathrm{T}^0$	unitless
C _d	Coefficient of discharge	$M^0L^0T^0$	unitless
c`, d`	Coefficients of relative sequent depth depend on relative roughness length	$M^0L^0T^0$	unitless
c``, d``	Coefficients of relative energy loss depend on relative roughness length	$M^0L^0T^0$	unitless
E ₁	The specific energy at the initial depth	$M^0L^1T^0$	cm
E ₂	The specific energy at the sequent depth	$M^0L^1T^0$	cm
$\mathbf{E}_{\mathbf{L}}$	The energy loss due to the jump	$M^0L^1T^0$	cm

E_L/E_1	The relative energy loss.	$M^0L^0T^0$	unitless
F ₁	The initial Froude number	$M^0L^0T^0$	unitless
$\mathbf{F_r}$	The resistance force due to roughness	MLT ⁻²	dyne
$\mathbf{F_{rr}}$	The relative roughness force resistance	$M^0L^0T^0$	unitless
G	Gate opening	$M^0L^1T^0$	cm
g	The gravitational acceleration	M ⁰ LT ⁻²	cm/sec ²
I	The roughness intensity	$M^0L^0T^0$	unitless
$L_{\rm b}$	The location of roughness with respect to the gate	M ⁰ LT ⁰	cm
L _b /Y ₁	The relative jump position	$M^0L^0T^0$	unitless
$L_{\rm j}$	The length of the hydraulic jump	M ⁰ LT ⁰	cm
L _j /Y ₁	The relative jump length.	$M^0L^0T^0$	unitless
$\mathbf{L_r}$	The roughness length	M ⁰ LT ⁰	cm
L _r /Y ₁	The relative roughness length	$M^0L^0T^0$	unitless
\mathbf{M}_1	The momentum force at the beginning of the jump	M.L.T ⁻²	dyne
\mathbf{M}_2	The momentum force at the end of	M.L.T ⁻²	dyne

	the jump		
P ₁	The hydrostatic pressure force at the beginning of the jump	M.L.T ⁻²	dyne
P ₂	The hydrostatic pressure force at the end of the jump	M.L.T ⁻²	dyne
q	The discharge per unit width	$M^0.L^2.T^{-1}$	cm ² /sec
r	The height of the bed roughness	M^0LT^0	cm
R	Correlation factor	$M^0L^0T^0$	unitless
$\mathbf{R}_{\mathbf{N}}$	Reynolds's number	$M^0L^0T^0$	unitless
\mathbf{V}_1	The average velocity at the beginning of the jump	M ⁰ L.T ⁻¹	cm/sec
V_2	The average velocity at the end of the jump	M ⁰ L.T ⁻¹	cm/sec
Y ₁	The initial depth of the hydraulic jump	M^0LT^0	cm
Y ₂	The sequent depth of the hydraulic jump	M^0LT^0	cm
Y ₂ /Y ₁	The relative sequent depth of the jump	$\mathrm{M}^0\mathrm{L}^0\mathrm{T}^0$	unitless
γ	The specific weight of water	ML ⁻² T ⁻²	dyne/cm ³

μ	The dynamic viscosity	$ML^{-1}T^{-1}$	poise
ρ	The□ mass density	ML-3T ⁰	gm/cm ³

LIST OF FIGURES

FIGURE (2-1) USBR TYPE III STILLING BASIN	8
FIGURE (2-2) USBR TYPE IV STILLING BASIN	
FIGURE (2-3) USBR TYPE IV STILLING BASIN	. 10
FIGURE (2-4) USBR TYPE IX STILLING BASIN	. 10
FIGURE (3-1) SKETCH FOR THE HYDRAULIC JUMP OVER THE STILLING BASIN.	. 20
FIGURE (4-1) THE FLUME	
FIGURE (4-2) ORIFICE METER CALIBRATION	. 35
FIGURE (4-3) THE ROUGHNESS DIMENSIONS	
FIGURE (4-4) THE 1-ST INTENSITY TESTED I=4.2701%	
FIGURE (4-5) THE SECOND INTENSITY I=7.267%	
FIGURE (4-6) THE THIRD INTENSITY I=11.9825%	
FIGURE (4-7) THE FOURTH INTENSITY I=14.662%	
FIGURE (4-8) THE LAST INTENSITY I=21.5686%	
Figure (4-9) the first roughness length L_R =120 cm	
FIGURE (5-1) WATER SURFACE CONFIGURATION AT Q=3584 CM ³ /S AND G=	
CM FOR DIFFERENT INTENSITIES	
Figure (5-2) Water Surface configuration at $Q=4300 \text{ cm}^3/\text{s}$ and $G=4300 \text{ cm}^3/\text{s}$	2.0
COMFORT DIFFERENT INTENSITIES	
FIGURE (5-3) WATER SURFACE CONFIGURATION AT Q=4300 CM ³ /S AND	
G=2.50 CM FOR DIFFERENT INTENSITIES	. 47
Figure (5-4) Water Surface configuration at $Q=4300 \text{ cm}^3/\text{s}$ and $G=$	3
CM FOR DIFFERENT INTENSITIES	. 48
Figure (5-5) Water Surface configuration at different Q and $G\!\!=\!\!3$	CM
FOR I=21.5686	. 48
FIGURE (5-6) THE RELATION BETWEEN THE RELATION BETWEEN RELATIVE	
JUMP LENGTH AND INITIAL FROUDE FOR SMOOTH BED	. 50
Figure $(5-7)$ the relation between relative jump length and initial	
Froude for I=4.2701%	. 50
Figure $(5-8)$ the relation between relative jump length and initial	,
FROUDE NUMBER FOR DIFFERENT I	
Figure (5-9) the relation between a, B factors and the intensity	. 52
Figure (5-10) the relation between relative jump length & intensity	ГΥ
FOR DIFFERENT F_1 AND CONSTANT $L_{\scriptscriptstyle R} = 120{\rm CM}$. 53
Figure $(5-11)$ the relation between relative jump sequent depth an	
INITIAL FROUDE NUMBER FOR SMOOTH BED	. 55
Figure $(5-12)$ the relation between relative jump sequent depth an	ID
INITIAL FROUDE NUMBER FOR I=4.2701%	. 55

FIGURE (5-13) A RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AND	
INITIAL FROUDE NUMBERS FOR DIFFERENT I	56
FIGURE (5-14) THE RELATION BETWEEN A AND I	57
FIGURE (5-15) THE RELATION BETWEEN B'AND I	57
Figure (5-16) the relation between Y_2/Y_1 and I for different Froudi	Е
NUMBER	58
FIGURE (5-17) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL	_
FROUDE NUMBER FOR SMOOTH BED	60
FIGURE (5-18) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL	_
FROUDE NUMBER FOR I=4.2701%	60
FIGURE (5-19) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL	_
FROUDE NUMBER FOR DIFFERENT I	61
FIGURE (5-20) THE RELATION BETWEEN A AND I	62
FIGURE (5-21) THE RELATION BETWEEN B ``AND I	62
FIGURE (5-22) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND	
INTENSITY FOR DIFFERENT FROUDE NUMBERS	63
FIGURE (5-23) WATER SURFACE CONFIGURATION AT Q=3584 CM ³ /S AND	
G=1.50 CM FOR DIFFERENT INTENSITIES	66
FIGURE (5-24) WATER SURFACE CONFIGURATION AT Q=4300 CM ³ /S AND	
G=2.00 CM FOR DIFFERENT ROUGHNESS LENGTHS	66
Figure (5-25) Water Surface Profile at $Q=4300 \text{ cm}^3\text{/s}$ and $G=2.50 \text{ cm}^3$	
FOR DIFFERENT ROUGHNESS LENGTHS	67
Figure (5-26) Water Surface Profile at $Q=4300 \text{ cm}^3\text{/s}$ and $G=3.0 \text{ cm}$	
FOR DIFFERENT ROUGHNESS LENGTHS	67
FIGURE (527) THE RELATION BETWEEN RELATIVE JUMP LENGTH AND INITIA	L
Froude number for L_R = 120cm	69
Figure $(5-28)$ the relation between relative jump length and initial	
Froude number for L_R = 91.6cm	69
Figure $(5-29)$ the relation between relative jump length and initial	
Froude number for all L _r	70
FIGURE (5-30) THE RELATION BETWEEN THE RELATIVE ROUGHNESS LENGTH AND C	71
FIGURE (5-31) THE RELATION BETWEEN THE RELATIVE ROUGHNESS LENGTH AND D	71
FIGURE (5-32) THE RELATION BETWEEN THE RELATIVE JUMP LENGTH AND TH	ΙE
RELATIVE ROUGHNESS LENGTH FOR DIFFERENT INITIAL FROUDE NUMBER	R
AND CONSTANT $I = 8.8524\%$	72
FIGURE (5-33) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AND	O
INITIAL FROUDE NUMBERS FOR L_R = 120cm	74
FIGURE (5-34) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH ANI	O
INITIAL FROUDE NUMBERS FOR $L_p=91.6$ CM	74

FIGURE (3-35) THE RELATION BETWEEN THE RELATIVE JUMP SEQUENT DEPTH
AND INITIAL FROUDE NUMBERS FOR ALL $L_{\scriptscriptstyle R}$
FIGURE (5-36) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AND
THE RELATIVE ROUGHNESS LENGTH FOR DIFFERENT INITIAL FROUDE
NUMBERS
FIGURE (5-37) THE RELATION BETWEEN RELATIVE JUMP ENERGY LOSS AND
INITIAL FROUDE NUMBER FOR L_R =120 cm
FIGURE (5-38) THE RELATION BETWEEN RELATIVE JUMP ENERGY LOSS AND
INITIAL FROUDE NUMBER FOR L_R =91.6CM
FIGURE (5-39) THE RELATION BETWEEN RELATIVE JUMP ENERGY LOSS AND
INITIAL FROUDE NUMBER FOR ALL $L_{\scriptscriptstyle R}$
FIGURE (5-40) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND THE
RELATIVE ROUGHNESS LENGTH FOR DIFFERENT F_1
FIGURE (5-41) DIMENSIONS OF THE STILLING BASIN FOR RECTANGULAR SHAPE
IN COMPARISON STATE
FIGURE (5-42) DIMENSIONS OF THE STILLING BASIN FOR T-SHAPE 82
Figure $(5-43)$ a comparison between the T-shape and the rectangular
SHAPE ACCORDING TO THE RELATIVE JUMP SEQUENT DEPTH
FIGURE (05-44) A COMPARISON BETWEEN THE T-SHAPE AND THE
RECTANGULAR SHAPE ACCORDING TO RELATIVE JUMP LENGTH 84
Figure $(5-45)$ a comparison between the T-shape and the rectangular
SHAPE ACCORDING TO THE RELATIVE ENERGY LOSS
FIGURE (5-46) COMPARISON BETWEEN THE SMOOTH BED AND THE DESIGNED STILLING BASIN
ACCORDING TO THE RELATIVE LENGTH OF JUMP86
FIGURE (5-47) COMPARISON BETWEEN THE SMOOTH BED AND THE DESIGNED STILLING BASIN
ACCORDING TO THE RELATIVE SEQUENT DEPTH OF THE HYDRAULIC JUMP
FIGURE (5-48) COMPARISON BETWEEN THE SMOOTH BED AND THE DESIGNED STILLING BASIN
ACCORDING TO THE RELATIVE ENERGY LOSS OF THE HYDRAULIC JUMP
FIGURE (5-49) SENSITIVITY ANALYSIS
FIGURE (B-1) THE RELATION BETWEEN RELATIVE JUMP LENGTH AND INITIAL
FROUDE NUMBER FOR I=7.2331%
FIGURE (B-2) THE RELATION BETWEEN RELATIVE JUMP LENGTH AND INITIAL
FROUDE NUMBER FOR I=11.9825%116
FIGURE(B-3)THE RELATION BETWEEN RELATIVE JUMP LENGTH AND INITIAL
FROUDE NUMBER FOR I=14.4662%
FIGURE (B-4) THE RELATION BETWEEN RELATIVE JUMP LENGTH AND INITIAL
FROUDE NUMBER FOR I=21.5686%117

FIGURE (B-5) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AND	
INITIAL FROUDE NUMBER FOR I= 7.2331%	.18
Figure $(B-6)$ the relation between relative jump sequent depth and	
INITIAL FROUDE NUMBER FOR $I=11.9825\%$.18
Figure $(B-7)$ the relation between relative jump sequent depth and)
INITIAL FROUDE NUMBER FOR $I=14.4662\%$.19
Figure $(B-8)$ the relation between relative jump sequent depth and	
INITIAL FROUDE NUMBER FOR $I=21.5686\%$.19
Figure (B-9) the relation between relative energy loss and initial	
FROUDE NUMBER FOR I=7.2331%	.20
Figure $(B-10)$ the relation between relative energy loss and initial	L
Froude number for I=11.9825%1	.20
Figure $(B-11)$ the relation between relative energy loss and initial	L
Froude number for I=14.4662%1	.21
FIGURE (B-12) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIA	L
Froude number for I=21.5686%1	.21
Figure $(B-13)$ the relation between relative jump length and initia	L
Froude number for L_R = 78.1cm	.22
Figure $(B-14)$ the relation between relative jump length and initia	
Froude number for L_R = 64.4cm	.22
Figure $(B-15)$ the relation between relative jump length and initia	L
Froude number for L_R = 50.2cm	.23
FIGURE (B-16) THE RELATION BETWEEN RELATIVE JUMP LENGTH AND INITIA	L
Froude number for L_R = 36.6cm	.23
FIGURE (B-17) THE RELATION BETWEEN RELATIVE JUMP LENGTH AND INITIA	
Froude number for L_R = 23.2cm	.24
FIGURE (B-18) THE RELATION BETWEEN RELATIVE JUMP LENGTH AND INITIA	L
FROUDE NUMBER FOR L_R = 9.2CM	.24
FIGURE (B-19) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AN	D
INITIAL FROUDE NUMBER FOR $L_{\text{R=}}78.1\text{CM}$.25
FIGURE (B-20) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AN	D
INITIAL FROUDE NUMBER FOR L_R =64.4CM	.25
FIGURE (B-21) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AN	D
INITIAL FROUDE NUMBER FOR L_R =50.2CM	.26
FIGURE (B-22) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AN	D
INITIAL FROUDE NUMBER FOR L_R =36.6CM	
FIGURE (B-23) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AN	
INITIAL FROUDE NUMBER FOR L_R =23.2CM1	

FIGURE (B-24) THE RELATION BETWEEN RELATIVE JUMP SEQUENT DEPTH AND
INITIAL FROUDE NUMBER FOR L_R =9.2CM127
FIGURE (B-25) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL
Froude number for $L_R = 78.1$ cm
FIGURE (B-26) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL
Froude number for L_R = 64.4cm
FIGURE (B-27) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL
FROUDE NUMBER FOR $L_R = 50.2$ CM
FIGURE (B-28) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL
FROUDE NUMBER FOR $L_R = 36.6$ CM
FIGURE (B-29) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL
Froude number for L_R = 23.2cm
FIGURE (B-30) THE RELATION BETWEEN RELATIVE ENERGY LOSS AND INITIAL
Froude number for L_R = 9.2cm
LIST OF PHOTOS:
Photo (4-1) the flume 31
Photo (4-1) the flume 31 Photo (4-2) side view of the Flume 33
Photo (4-2) side view of the Flume
Photo (4-2) side view of the Flume
Photo (4-2) side view of the Flume

Abstract

The stilling basins are commonly used to dissipate the energy and protect the down stream floor from erosion. Several researchers studied the efficiency of the stilling basins and how to improve their efficiency. The aim of the present work is to improve the roughened stilling basin using T-shape roughness instead of rectangular shape roughness and then design this new shape of roughness. In order to design the new stilling basin an experimental work was carried out. Five different intensities and eight different lengths were tested under four gate openings and six different flows for each gate opening. The experiments were carried out in the hydraulics laboratory of the Faculty of Engineering Ain Shams University. As a result of the present work the best intensity ranged between 7.2 to 8.8 % and the best roughness length as L_r/Y_1 =16 where L_r = roughness length and Y_1 = initial depth. The T-shape roughness save materials and reduce the jump length compared to the rectangular shape of roughness.

Chapter 1

INTRODUCTION

Irrigation structures have a great importance in our life allover the world. The irrigation heading up structures can be classified mainly into two categories: high head structures (such as dams and spillways) and low head structures (such as regulators and weirs). The problem is the excess energy that results from constructing these structures and the erosive action which happens downstream these structures due to this energy. So, heading up structures must be followed by energy dissipators to prevent the scour and erosion downstream such structures.

Hydraulic jump is considered as a powerful energy dissipator. Mainly it's formed downstream the hydraulic structure to convert the flow from supercritical flow to subcritical flow. But the hydraulic jump causes turbulence and apron erosion, so stilling basins are used to protect the downstream apron from erosion by dissipating the excess energy by the generated friction in terms of stilling basin blocks. The stilling basin blocks are arranged in a staggered way to make the path of high energy water longer to dissipate more energy.

As a matter of fact, the length of the stilling basin of a hydraulic jump should be long enough to permit the flow to regain its normal depth and velocity before the earthen section. Thus minimizing the length of the floor of the stilling basin is one of the important considerations from the economical point of view.

1.1 Scope of Work

The present experimental research aims at improving the efficiency of the stilling basins using a new shape of roughness elements (T-shape) from both the economical and hydraulic point of views and finding out the best intensity and length for the used shape. Such research would be carried out using physical model for the testing stilling basin.

1.2 Objectives

The main objectives of the present study may be summarized as follows:

- 1. Investigating theoretically and experimentally the flow over stilling basin using a new roughness shape.
- 2. Studying the flow characteristics and water surface profile along the stilling basin.
- 3. Determining the change in flow characteristics due to change in intensity and length of roughness.
- 4. Finding out the best length and the best intensity for the new shape of roughness.
- 5. Comparing between the new shape of roughness and the ordinary shape of roughness (rectangular shape).
- 6. Finding out which shape is more efficient and economic.
- 7. Calculating the efficiency of the designed stilling basin.

1.3 Plan of Study:

The study comprises six chapters that can be demonstrated as follows: