







شبكة المعلومـــات الجامعية التوثيق الالكتروني والميكروفيا.



جامعة عين شمس

التوثيق الالكتروني والميكروفيلم



نقسم بللله العظيم أن المادة التي تم توثيقها وتسجيلها على هذه الأفلام قد اعدت دون آية تغيرات



يجب أن

تحفظ هذه الأفلام بعيداً عن الغبار

40-20 في درجة حرارة من 15-20 منوية ورطوبة نسبية من

To be kept away from dust in dry cool place of 15 – 25c and relative humidity 20-40 %









EXPERIMENTAL AND THEORETICAL DETERMINATION OF PHYSICAL PROPERTIES OF CO2/HYDROCARBON MIXTURES FOR ENHANCED OIL RECOVERY

À Dissertation by ID KAMEL ELSAYED SALEM Submitted to Suez Canal University for the degree of

DOCTOR OF PHILOSOPHY

A. Bayoursi S. Ayout Should Sha laby

Supervised By

Prof. Dr. Hammed M. Khatab (Chair of Committee)

Department of Petroleum Engineering Faculty of Petroleum and Mining Engineering

Suez, Egypt

Dr. Elsayed D. Elayouty (Member)

Department of Petroleum Engineering Suez, Egypt

المدر يز جنب

Dr. Maria A. Barrufet (Co-Chair of Committee)

Department of Petroleum Engineering Texas A &M University U.S.A.

M. A. Tantawy

Dr. Mahmoud Abdu Tantawy (Member)

Department of Petroleum Engineering Suez, Egypt

ABSTRACT

CO₂ flooding is considered to have multi-contact miscibility displacement mechanisms. It changes the reservoir fluid in a complex manner. This type of Enhanced Oil Recovery (EOR) technique is very economically viable, readily available, and environmentally acceptable. CO₂ flooding is one of the EOR techniques in the gas processes category.

In evaluating a field for possible CO₂ flooding certain data are required that can either be measured in the laboratory or, in the absence of measurements, be estimated from fundamental and theoretical considerations. The required data include the following: a) Minimum miscibility pressure (MMP), b) Swelling of crude oil, c) Viscosity reduction.

Miscibility is defined as physical condition between two or more fluids that will permit them to mix in all proportions without the existence of an interface. The minimum pressure required to achieve a multi-contact miscibility between injected fluid and oil, specifically, is called the minimum miscibility pressure (MMP).

The CO_2 MMP is an important parameter for screening and selecting reservoirs for CO_2 injection project to simulate reservoir performance as a result of CO_2 injection.

The objectives of this study were separated into two parts. The first one was to predict the MMP using different correlations available in the literature i.e. Petroleum Recovery Inst., Yellig, GlasØ, Alston, and Orr. The thermodynamic MMP was also evaluated using an EOS (Equation Of State). The simulator (PEPPER) was used to obtain the bubble-points and dew-points, based on this data, the thermodynamic minimum miscibility pressures are determined using pseudo ternary diagram. This simulator uses Soave-Redlich-Kwong (SRK) equation of state (58). The MMP coincides with the plait point, i.e. critical point.

The second part of the objectives is an experimental study. (1) A laboratory study for three types of synthitic oil is set up and experimental procedures were developed using

toluene in the calibration experiment and three types of Hydrocarbon/Carbon dioxide mixtures in the main experiment. (2) Determine CO₂/hydrocarbon systems viscosities at high temperatures and pressures using a high pressure rolling ball viscometer and compare these viscosities with those predicted from Lohrenz-Bray-Clark (LBC), Lansangan and Sandler models in the literature. The same types of oil were used to measure the viscosities.

Results from studies with synthetic oils show that large oil recoveries were obtained at pressures more than the minimum miscibility pressure (MMP). The average oil recoveries were about of the 90 % OOIP (1.2 PV of CO₂ injected).

We have also concluded from these studies, that (1) There was little or no effect of oil composition on the CO₂ MMP (2) A comparative investigation was performed between the experimental results of this study and six different correlations provided in the literature. The comparisons show a good agreement with each of Yellig and Orr correlations. (3) Viscosities for hydrocarbon/CO₂ mixtures were measured and compared with the published values (Cullick, Mathis, Orbey and Sandler). It has been found that the technique is sufficiently accurate for engineering measurement on crude oil systems.(4) According to the comparison between Lohrenz-Bray-Clark (LBC) correlation (which is widely used in oil industry) and the present experimental results, it was found that LBC viscosities are very much lower than the measured values specially at high concentrations of CO₂. Accordingly, such correlation is not recommended to be used.

Finally, a) according to screening pressures of several Egyptian oil reservoirs, it was found that the majority of these reservoirs are not candidates for CO₂ miscible flooding because their current pressures are less than CO₂ MMP. However, Ras Budran field was found to be suitable for such flooding (current pressure is greater than MMP). b) according to the performed theoretical calculations, if CO₂ flooding had been applied on Ramadan oil field at its initial pressure, oil viscosities would have decreased and hence the recovery factor would have increased.

DEDICATION

This dissertation is lovingly dedicated to my parents, who patiently endured its preparation, and to my wife, for her encouragement, understanding, and devotion and my lovely daughters Aisha and Fatma and my son Mohamed

ACKNOWLEDGMENTS

I would like to thank all members of my family for their concern and support.

I would like to express my sincere thanks to Dr. Maria A. Barrufet for her trust in me to conduct her first research project in Department of Petroleum Engineering at Texas A & M university. I thank her for her guidance through the research. At the very first meeting that we had, she told me that everything can be accomplished as long as we have perseverance. Perseverance does help a lot.

A special thanks to Prof. Dr. Hamed M. Khattab for serving on my advisory committee. I really appreciate the suggestions and comments given to improve my dissertation. Special thanks to Prof. Dr. Shouhdi El-Maghraby Shalaby, Head of the Petroleum Engineering Department for his assistance, guidance and advise during preparing this research.

I would also like to thank Dr. Elsayed D. Elayouty and Dr. Mahmoud Abdou Tantawy for serving on my advisory committee.

I would like to thank all the staff members of the Department of Petroleum Engineering, the Faculty of Petroleum and Mining Engineering for the help they provided during my study.

A special thanks to Dr. Mohamed Abd Eltawab Elgindy, Dean of the Faculty of Petroleum and Mining Engineering for his advice and moral support. I would also like to thank my friends for giving me the moral support during my tough days and many thanks to laboratory technician Matt for the help he provided me during the experimental work.

I would also like to thank all the staff members of the Department of Petroleum Engineering at Texas A & M University for providing me with education and encouragement to complete this work.

TABLE OF CONTENTS

| Page |
|--|
| ABSTRACTi |
| DEDICATIONi |
| ACKNOWLEDGMENTSv |
| TABLE OF CONTENTSvi |
| LIST OF TABLESxi |
| LIST OF FIGURESxv |
| 1. INTRODUCTION |
| 1.1. BACKGROUND1 |
| 1.1.1. Miscibility Definition and Description1 |
| 1.1.2. Classifications of Miscible Displacement Processes2 |
| 1.1.3. Screening Criteria for Identifying Reservoir with Miscible Flooding6 |
| 1.1.4. Miscible Displacement by CO ₂ 8 |
| 1.1.5. Minimum Miscibility Pressure (MMP) 10 |
| 1.1.6. MMP Correlation Background11 |
| 1.1.7. Effect of Miscible Displacement by CO ₂ on Oil Viscosity12 |
| 1.2. PURPOSES AND OBJECTIVES13 |
| 1.3. STATEMENT OF PROBLEM14 |
| 2. REVIEW OF THE LITERATURE |
| 2.1. INTRODUCTION TO EOR PROCESSES |
| 2.2. GUIDELINES FOR IDENTIFYING RESERVOIRS WITH ${\rm CO_2}$ MISCIBLE FLOODING POTENTIAL |

| Page |
|---|
| 2.3. PRINCIPALS OF CO ₂ MISCIBLE FLOODING |
| 2.4. BACKGROUND OF LABORATORY DETERMINATION OF CO ₂ MMP |
| 2.4.1. Displacement Test for Measuring CO ₂ MMP by Miscibility Apparatus |
| 2.4.2. How to Saturate the Tube with Oil20 |
| 2.4.3. How to Pressurize and Collect a Sample20 |
| 2.5. CRITERIA FOR MISCIBILITY AND DETERMINATION OF CO ₂ MMP |
| 2.5.1. Miscibility Criteria21 |
| 2.5.2. Two-Phase Production in Miscible CO ₂ Displacement21 |
| 2.6. CORRELATION OF MMP's22 |
| 2.6.1. Petroleum Recovery Inst. Correlation22 |
| 2.6.2. Yellig and Metcalf Correlation22 |
| 2.6.3. GlasØ Correlation24 |
| 2.6.4. Alston et al Correlation25 |
| 2.6.5. Orr and Sliva Correlation27 |
| 2.7. RECENT DEVELOPMENTS IN EQUATION OF STATE29 |
| 2.8. CALCULATION OF THERMODYNAMIC MMP's (SRK EQUATION OF STATE)31 |
| 2.9. CORRELATION OF VISCOSITIES33 |
| 2.9.1. Lohrenz-Bray-Clark (LBC) Correlation33 |
| 2.9.2. Lansangan Correlation38 |
| 2.9.3. Sandler Model39 |

| Page | e |
|---|---|
| 3. PREDICTION OF MMP'S BY USING CORRELATIONS AND EOS FOR CO ₂ /HYDROCARBON SYSTEMS | |
| 3.1.INTRODUCTION42 | |
| 3.2. PREDICTION OF MMP's | |
| 3.2.1. MMP's Predicted from Petroleum Recovery Inst.Correlations43 | |
| 3.2.2. MMP's Predicted from Yellig Correlation43 | |
| 3.2.3. MMP's Predicted from GlasØ Correlation | |
| 3.2.4. MMP's Predicted from Alston Correlation48 | |
| 3.2.5. MMP's Predicted from Orr and Silva Correlation48 | |
| 3.2.6. MMP's Predicted from Thermodynamic Equation of State (SRK EOS) | |
| 3.3. DISCUSSION55 | |
| 4. RECOMMENDED APPARATUS AND EXPERIMENTAL SET UP | |
| PART I- JEFRI SLIM-TUBE APPARATUS72 | |
| 4.1. INTRODUCTION | |
| 4.2. THE APPARATUS72 | |
| 4.2.1. Vacuum System72 | |
| 4.2.2. Hydraulic System73 | |
| 4.2.3.Slim-Tube Apparatus74 | |
| 4.3. SPECIFICATIONS76 | |
| 4.4. THE EXPERIMENTAL SET-UP77 | |
| 4.5 TEST PROCEDURE 77 | |

| | Page |
|---|------|
| 4.5.1. Calibration | .77 |
| 4.5.2. Sample Preparation | .80 |
| 4.6. TEST PREPARATION | .80 |
| 4.6.1. Back Pressure Regulator and Sight Glass Overburden Pressure | .81 |
| 4.6.2. Saturation of Slim-Tube | 81 |
| 4.6.3. Solvent Preparation | 82 |
| 4.7. RUNNING AN EXPERIMENT | 82 |
| PART II- RUSKA HIGH PRESSURE ROLLING BALL VISCOMETER | 82 |
| 4.8. INTRODUCTION | 83 |
| 4.9. THEORY OF OPERATION | 33 |
| 4.10. DESCRIPTION OF SYSTEM | 34 |
| 4.10.1. Mechanical Test Assembly | 34 |
| 4.10.2.Control Unit With Instrument Panel | 34 |
| 4.11. CALIBRATION PROCEDURES | 84 |
| 4.12. EXPERIMENTS WITH HYDROCARBON AND HC/ CO ₂ SYSTEMS | 86 |
| 4.12.1. The Oil Mixtures | 86 |
| 4.12.2. The Experimental Procedure | .86 |
| 4.12.3. Density Calculation | 90 |
| 5. RESULTS AND DISCUSSIONS OF THE EXPERIMENTS | |
| PART-I- Results and Discussions of Slim-Tube Experiment | 91 |
| 5.1. The Calibration Experimentation | .91 |
| 5.2. Experiments with CO ₂ and Hydrocarbon | 91 |

| | Page |
|--|-------|
| 5.2.1. Slim-Tube Miscible Displacement Run | 91 |
| 5.2.2. Determination of CO ₂ MMP from Slim Tube Apparatus | 96 |
| 5.3. Miscibility Criteria Limitations | 107 |
| 5.4. Effect of Oil Composition | 101 |
| 5.5. Comparison Between Predicted and Measured MMP's | 110 |
| PART-II. Results and Discussion of viscosity Experiment | 124 |
| Theoretical Field Implementation of CO2 Flooding | 140 |
| 6. CONCLUSIONS AND RECOMMENDATIONS | • |
| 6.1. CONCLUSIONS | 149 |
| 6.2. RECOMMENDATIONS | 149 |
| NOMENCLATURE | 151 |
| REFERENCES | . 152 |
| APPENDIX (A) | 157 |
| APPENDIX (B) | 162 |
| APPENDIX (C) | 168 |
| APPENDIX (D) | 172 |
| APPENDIX (E) | 192 |
| Arabic Summary | |