



OPTIMIZATION OF FRICTION STIR SPOT WELDING PARAMETERS FOR 7075 AND 6061 ALUMINUM ALLOYS USING TAGUCHI METHOD

By

Mohamed Mohamed Azzam Abdallah

A Thesis Submitted to the
Faculty of Engineering at Cairo University
In Partial Fulfillment of the
Requirements for the Degree of
MASTER OF SCIENCE
In
Metallurgical Engineering

OPTIMIZATION OF FRICTION STIR SPOT WELDING PARAMETERS FOR 7075 AND 6061 ALUMINUM ALLOYS USING TAGUCHI METHOD

By Mohamed Mohamed Azzam Abdallah

A Thesis Submitted to the
Faculty of Engineering at Cairo University
In Partial Fulfillment of the
Requirements for the Degree of
MASTER OF SCIENCE
In
Metallurgical Engineering

Under the Supervision of

| Prof. | Dr. | Wa | leed | Mohame | ed |
|-------|-----|----|-------|--------|----|
| | | Kh | alifa | 1 | |
| Α . | A A | 1 | 1 | 0 | |

Professor of Metallurgical Engineering
Mining, petroleum, and metallurgical
Department
Faculty of Engineering, Cairo University

Dr. Amer Ahmed Abdel-Hakeem

Assistant Professor Industrial, and Management Engineering The Higher Institute of Engineering 6th of October City

والمالات

FACULTY OF ENGINEERING, CAIRO UNIVERSITY
GIZA, EGYPT
2018

OPTIMIZATION OF FRICTION STIR SPOT WELDING PARAMETERS FOR 7075 AND 6061 ALUMINUM ALLOYS USING TAGUCHI METHOD

By Mohamed Mohamed Azzam Abdallah

A Thesis Submitted to the
Faculty of Engineering at Cairo University
In Partial Fulfillment of the
Requirements for the Degree of
MASTER OF SCIENCE
In
Metallurgical Engineering

| Approved by the | |
|---|---------------------|
| Examining Committee | |
| | 9 100 100 100 100 |
| Prof. Dr. Waleed Mohamed Khalifa. | Thesis Main Advisor |
| Prof. Dr. Mohamed Raafat El kousy. | Internal Examiner |
| Prof. Dr. Morsi Ameen Abo khalaah. | External Examiner |
| (Central Metallurgical R&D Institute (CMRDI)) | Morsy Amin |

FACULTY OF ENGINEERING, CAIRO UNIVERSITY GIZA, EGYPT 2018 **Engineer's Name:** Mohamed Mohamed Azzam abdallah

Date of Birth: 15 / 11 / 1986 **Nationality:** Egyptian

E-mail: Eng_azzam60@yahoo.com

Phone: 01112618643

Address: 38 El Masraf Street, Ezbet madkour, Giza

Registration Date: 1/10/2014 **Awarding Date:**/2018 **Degree:** Master of Science

Department: Mining, Petroleum, and metallurgy engineering

Supervisors:

Prof. Dr. Waleed Mohamed Khalifa Dr. Amer Ahmed Abdel-Hakeem

(Industrial, and Management Engineering

The Higher Institute of Engineering 6th of October City)

Examiners:

Prof. Dr. Waleed Mohamed Khalifa Prof. Dr. Mohamed Raafat El Kousy Prof. Dr. Morsi Ameen Abo khalaah

(Central Metallurgical R&D Institute (CMRDI))

Title of Thesis:

Optimization of Friction Stir Spot Welding Parameters for 7075 and 6061 Aluminum alloys Using Taguchi Method

Key Words:

FSSW, 7075-T6, 6061-T6, Anvil, Taguchi method

Summary:

Friction stir welding is a solid-state welding process, where there is no melting taking place. In this study, a friction stir spot welding process was developed. The aim of this work was to optimize the process parameters of welding AA7075-T6 and AA6061-T6, separately. Rotational speed, pin profile, plunge depth, and shape of anvil were the main parameters studied. The experimental results showed that the optimal levels found to be 800 rpm, triangular pin, 1 mm, and convex anvil for AA7075-T6; and were 500 rpm, square pin, 1 mm, and convex anvil for AA6061-T6, respectively. The worst joint properties were observed for a rotational speed of 1250 rpm, and rounded pin profile and 1.5 mm plunge depth, with flat anvil for both alloys. ANOVA results revealed that the pin profile is the dominant parameter in the process, followed by the plunge depth, then the anvil shape and the last parameter was the rotational speed. The percentages of contribution were 54%, 21%, 14, and 11%, respectively, for the AA7075-T6 alloy. For the 6061-T6 alloy, it was found that the pin profile was most effective FSSW process parameter, followed by anvil shape, plunge depth and the rotational speed. The percentages of contribution were 51%, 35%, 8, and 6%, respectively.



Disclaimer

I hereby declare that this thesis is my own original work and that no part of it has been submitted for a degree qualification at any other university or institute.

I further declare that I have appropriately acknowledged all sources used and have cited them in the references section.

Name: Mohamed Mohamed Azzam

Date: 16/09/2018

Signature: M.A33am

Acknowledgments

First of all, I would like to express my sincere appreciation and gratitude to my supervisors, Prof. Dr. Waleed Khalifa and Dr. Amer Ahmed for their kind supervision, encouragement, and supporting during my study, also I want to thank every member in mechanical testing lab of metallurgical department at Cairo university for their help, with special thanks for Eng. Mohamed Hafez and Eng. Ali Elasheri. In addition, I would like to thank my colleagues Eng. Ayman Selim and Eng. Ahmed Sayed for their help.

I also wish deeply thank for Hongbo machinery company (HMC), Nantong, China, especially Eng. Feng for offering the machine, which without it the work would have not been achieved.

Finally, I want to express my warm gratitude to my mother and my wife for their supporting, inspiration, and motivation through the years of the study.

Table of Contents

| ACKNOWLEDGMENTS | I |
|---|------|
| LIST OF TABLES | V |
| LIST OF FIGURES | VI |
| NOMENCLATURE | VIII |
| ABSTRACT | IX |
| CHAPTER 1: INTRODUCTION | 1 |
| CHAPTER 2: LITERATURE REVIEW | 3 |
| 2.1 ALUMINUM AND ITS ALLOYS | 3 |
| 2.2. DESIGNATION OF ALUMINUM ALLOYS | 4 |
| 2.2.1. Wrought alloys | 4 |
| 2.2.2. Casting alloys | 4 |
| 2.3. THE EFFECTS OF ALLOYING ELEMENTS IN ALUMINUM | 4 |
| 2.4. Temper Designation | 5 |
| 2.4.1. Temper Designations Non-heat treatable Alloys | 6 |
| 2.4.2. Temper Designations Heat-Treatable Alloys | |
| 2.5. HIGH STRENGTH ALUMINUM ALLOYS | |
| 2.5.1. 7xxx Al-Zn Alloys | |
| 2.5.1.1.7075 Aluminum alloys | |
| 2.5.2. 6xxx Al-Mg-Si Alloys | |
| 2.5.2.1 6061 Aluminum alloys | |
| 2.6. THE METHODS OF JOINING HIGH STRENGTH ALUMINUM ALLOYS | |
| 2.6.1. Resistance Spot Welding (RSW) | 10 |
| 2.6.2. Self-Piercing Riveting (SPR) | 12 |
| 2.6.3. Friction stir welding (FSW) | 13 |
| 2.6.3.1 Friction stir spot welding (FSSW) | |
| 2.6.3.2. Microstructure characterization in FSSW | 15 |
| 2.7. COMPARISON BETWEEN FSSW, RSW, AND SPR | 17 |
| 2.8. TAGUCHI METHOD | 18 |
| CHAPTER 3: EXPERIMENTAL WORK | 20 |
| 3.1. Experimental procedure | 20 |
| 3.2. The Material | 22. |

| 3.3. The equipment | 23 |
|--|----|
| 3.4 Preparation of the rotating tool | 24 |
| 3.5 The anvil | 28 |
| 3.6 Preparation of the samples | 29 |
| 3.7 WELDING PROCEDURE | 33 |
| 3.8 MECHANICAL CHARACTERIZATION | 34 |
| 3.8.1. Lap shear strength test (LSS Test) | 34 |
| 3.9 METALLURGICAL CHARACTERIZATION | 37 |
| CHAPTER 4: RESULTS AND DISCUSSION | 41 |
| 4.1 PARAMETERS OPTIMIZATION | 41 |
| 4.1.1 DoE: Taguchi L9 orthogonal array | 41 |
| 4.1.2 Optimization of LSS and S/N ratio | 42 |
| 4.1.2.1 Optimization of LSS and S/N ratio for 7075-T6 | 43 |
| 4.1.2.2 Optimization of LSS and S/N ratio for 6061-T6 | 43 |
| 4.1.3 The main effects of design parameters | 44 |
| 4.1.3.1 The main effects of design parameters for AA7075-T6 | 44 |
| 4.1.3.2 The main effects of design parameters for AA6061-T6 | 45 |
| 4.1.4 Analysis of variance (ANOVA) | 47 |
| 4.1.4.1 Analysis of variance (ANOVA) for 7075-T6 | 48 |
| 4.1.4.2 Analysis of variance (ANOVA) for 6061-T6 | 50 |
| 4.1.5 Prediction for optimum quality performance for 7075-T6 and 6061-T6 | 51 |
| 4.2. MICROSTRUCTURAL CHARACTERIZATION | 53 |
| 4.2.1. Microstructural characterization for 7075-T6 | 53 |
| 4.2.2. Microstructural characterization for 6061-T6 | 60 |
| 4.3. Fracture analysis | 65 |
| 4.3.1. Fracture analysis for 7075-T6 | 66 |
| 4.3.2. Fracture analysis for 6061-T6 | 67 |
| CHAPTER 5: CONCLUSIONS | 68 |
| REFERENCES | 71 |

List of Tables

| Table 2.1: The major elements in aluminum alloys | 4 |
|---|------|
| Table 2.2: The role of the alloying elements in aluminum alloys | 5 |
| Table 2.3: Temper designations for wrought alloys | 6 |
| Table 2.4: Designations for strain hardened alloy | 6 |
| Table 2.5: Designation for the heat treatable alloys | 7 |
| Table 2.6: Key benefits of friction stir welding | . 13 |
| Table 2.7: Taguchi orthogonal array selector | . 18 |
| Table 3.1: Summary of the experimental work program presented through this | |
| research. | . 20 |
| Table 3.2: Chemical composition for 7075-T6, and 6061-T6 (wt %) | . 22 |
| Table 3.3: Mechanical properties for AA7075-T6, and 6061-T6 (measured) | . 22 |
| Table 3.4: Chemical composition for H13 (wt %) | . 24 |
| Table 3.5: Mechanical properties for H13 | . 24 |
| Table 3.6: Dimensions of the rotating tool | . 26 |
| Table 3.7: Welding parameters and their levels. | . 33 |
| Table 3.8 (a): Orthogonal array of Experiment. | . 33 |
| Table 3.8(b): Orthogonal array of Experiment. | . 34 |
| Table 3.9: Technical specification of tensile machine. | . 35 |
| Table 3.10: The selected conditions for investigation | |
| Table 3.11: Chemical composition of the used etchant. | . 39 |
| Table 4.1: Taguchi's array for parameters and their levels | |
| Table 4.2: The mean and S/N ratio for LSS (7075-T6) | |
| Table 4.3: The mean and S/N ratio for LSS (6061-T6) | . 43 |
| Table 4.4: The main effects of parameters on mean LSS and S/N ratio for AA7075- | ·T6 |
| | . 44 |
| Table 4.5: The main effects of parameters on mean LSS and S/N ratio for AA6061- | -T6 |
| | . 46 |
| Table 4.6: Results of ANOVA for mean LSS (7075-T6) | |
| Table 4.7: Results of ANOVA for S/N ratio (7075-T6) | |
| Table 4.8: Results of ANOVA for mean LSS (6061-T6) | |
| Table 4.9: Results of ANOVA for S/N ratio (6061-T6) | |
| Table 4.10: the results for the predicted optimized performance 7075-T6, and 6061- | -T6 |
| | . 52 |

List of Figures

| Figure 2.1: Stress-Strain Curves of Aluminum in Comparison with Various Metals | |
|---|-----|
| and Alloys | 3 |
| Figure 2.2: Density-Related Strength of aluminum in Comparison with Various | |
| Metals and Alloys | 8 |
| Figure 2.3: Weldability of various aluminum alloys | 10 |
| Figure 2.4: Schematic of resistance spot welding | 11 |
| Figure 2.5: Self-piercing riveting process | |
| Figure.2.6: Mazda RX-8 Rear Door (Aluminum Panel) is made by FSSW | 14 |
| Figure.2.7: An FSSW tool with the shoulder and pin identified | |
| Figure 2.8: Schematic illustration of Friction Stir Spot Welding process | 15 |
| Figure 2.9: Illustration of microstructural regions in FSSW | 16 |
| Figure 3.1: Flowchart of the different work stages | 21 |
| Figure 3.2: The vertical milling machine | 23 |
| Figure 3.3: The clamping device. | 23 |
| Figure 3.4: Dimensions of the pin: a) different pin profiles, b) Total length of the | |
| rotating tool, c) shoulder diameter, and d) pin diameter | 25 |
| Figure 3.5: Schematic of dimensions of the rotating tool | 26 |
| Figure 3.6: pin preparation: a) Flame hardening technique, b) Measurement of the | |
| temperature before quenching, c) Average hardness value after quenching, d) Hardness | ess |
| measurement | 27 |
| Figure 3.7: Anvil profiles: a) Flat anvil, b) Convex anvil, c) Concave anvil, d) | |
| Location of the anvil in the clamping device | 28 |
| Figure 3.8: Dimensions of the anvil profiles: a) flat anvil, b) convex anvil, and c) | |
| concave anvil. | 29 |
| Figure 3.9: Material sheet | 29 |
| Figure 3.10: Preparation of specimens, a) The cutting machine, b) The cutting | |
| process, c) The dimensions of one piece after cutting | 30 |
| Figure 3.11: Schematic of lap tensile specimen. | 31 |
| Figure 3.12: Holding the specimen by the clamping device. | 32 |
| Figure 3.13: LSS test specimen after welding | |
| Figure 3.14: SHT 4605 tension machine. | 35 |
| Figure 3.15: The location of the spacers on the specimen | 35 |
| Figure 3.16: LSS specimen after shear test with separation | 36 |
| Figure 3.17: LSS specimen after shear test without separation | 36 |
| Figure 3.18: illustration of wire cut machine. | 37 |
| Figure 3.19: Cross section after cutting by wire cut machine: a) Top view, b) Side | |
| view | 38 |
| Figure 3.20: illustration of polishing process. | 38 |
| Figure 3.21: Olympus SC30 optical microscope used in microstructure investigation | 1. |
| | 39 |
| Figure 3.22: FEI Scanning electron microscope. | 40 |

| Figure 4.1: Effect of RS on LSS and S/N ratio |
|---|
| Figure 4.2: Effect of pin profile on LSS and S/N ratio |
| Figure 4.4: Effect of anvil shape on LSS and S/N ratio |
| Figure 4.3: Effect of penetration depth on LSS and S/N ratio |
| Figure 4.6: Effect of pin profile on LSS and S/N ratio |
| Figure 4.5: Effect of RS on LSS and S/N ratio |
| Figure 4.8: Effect of anvil shape on LSS and S/N ratio |
| Figure 4.7: Effect of penetration depth on LSS and S/N ratio |
| Figure 4.9: Percentage of Contribution for each parameter in: a) mean LSS and b) S/N |
| ratio (7075-T6) |
| Figure 4.10: Percentage of Contribution for each parameter in: a) mean LSS and b) |
| S/N ratio (6061-T6) |
| Figure 4.11: Cross sectional macrograph for: a) The best condition (5), b) The worst |
| condition (7) |
| Figure 4.12: microstructure at SZ for condition (5) at different magnifications (a) 50x |
| (b) 100x (c) 200x (d) 500x |
| Figure 4.13: The optical macrograph at SZ for condition (7) at different |
| magnifications (a) 50x (b) 100x (c) 200x (d) 500x |
| Figure 4.14: The optical micrograph for all regions SZ, TMAZ, and HAZ in condition |
| (5) |
| Figure 4.15: The optical micrograph for all regions SZ, TMAZ, and HAZ in condition |
| (7) |
| Figure 4.16: Scanning electron micrograph for the best condition (condition 5) 59 |
| Figure 4.17: Scanning electron micrograph for the worst condition (7) |
| Figure 4.18: Cross sectional macrograph for the best condition (condition9) |
| Figure 4.19: Cross sectional macrograph for the worst condition (condition7) 61 |
| Figure 4.20: The optical micrograph for all regions in the best condition (condition 9): |
| a): SZ, b): SZ-TMAZ-HAZ, c): BM, and d): The hook |
| Figure 4.21: The optical micrograph for all regions in the worst condition (condition |
| 7): a): SZ, b): SZ-TMAZ-HAZ, c): BM and d): The hook |
| Figure 4.22: Scanning electron micrograph for the best condition (9) |
| Figure 4.23: Scanning electron micrograph for the worst condition (7) |
| Figure 4.24: Fracture surfaces: a) mixed fracture mode (condition 5); b) Shear fracture |
| mode (condition 7) |
| Figure 4.25: Fracture surfaces: a) mixed fracture mode (condition 9), b) Shear fracture |
| mode (condition 7) |

Nomenclature

ANOVA Analysis of variance

BM Base material

DOE Design of experiment

DT Dwell time

FSSW Friction Stir Spot Welding
FSW Friction Stir Welding
HAZ Heat affected zone
LSS Lap shear strength
OM Optical microscope

PD Plunge depth RS Rotational speed

RSW Resistance Spot Welding SEM Scanning electron microscope

SPR Self-Piercing riveting SCC Stress corrosion cracking

SZ Stir zone Tm Melting point

TMAZ Thermo- mechanically affected zone

TWI The welding institute
TIG Tungsten Inert Gas
MIG Metal Inert Gas

 W_{eff} Effective weld width T_{eff} Effective sheet thickness

Abstract

Friction stir welding is a solid-state welding process, where there is no melting taking place. In this study, a friction stir spot welding process was developed. The aim of this work was to optimize the process parameters of welding AA7075-T6 and AA6061-T6, separately. Rotational speed, pin profile, plunge depth, and shape of anvil were the main parameters studied. The experimental results showed that the optimal levels found to be 800 rpm, triangular pin, 1 mm plunge depth, and convex anvil for AA7075-T6; and were 500 rpm, square pin, 1 mm plunge depth, and convex anvil for AA6061-T6, respectively. The worst joint properties were observed for a rotational speed of 1250 rpm, and round pin profile and 1.5 mm plunge depth, with flat anvil for both alloys. ANOVA results revealed that the pin profile is the dominant parameter in the process, followed by the plunge depth, then the anvil shape and the last parameter was the rotational speed. The percentages of contribution were 54%, 21%, 14, and 11%, respectively, for the AA7075-T6 alloy. For the AA6061-T6 alloy, it was found that the pin profile was most effective FSSW process parameter, followed by anvil shape, plunge depth and the rotational speed. The percentages of contribution were 51%, 35%, 8, and 6%, respectively.

Keywords: FSSW, 7075-T6, 6061-T6, Anvil, Taguchi method

Chapter 1: Introduction

Nowadays, there is a great challenge for developing and improving advanced welding techniques, to reduce the weight, increase the strength, and enhance the performance especially in automotive industries, ship building, and aerospace. Friction stir is one of these welding techniques that solves the problem of joining high strength aluminum alloys. These aluminum alloys are difficult to weld by traditional fusion welding such as TIG and MIG, especially in 2xxx and 7xxx series of aluminum alloys. FSW gave great results in improving of the mechanical properties and microstructure. It has been reported that fuel consumption can be decreased by 5.5% for each 10% reduction in weight of the vehicle and a one-pound reduction in the weight of a car would decrease carbon dioxide emissions by 20 pounds over the life of the vehicle [1].

FSSW has been developed by Mazda Motor Corp and Kawasaki Heavy Industries [2]. FSSW technique was first used in the Mazda RX-8 rear door panel spot welding in 2003 [3]. Mazda claimed that the reduction in consumption of the energy by 99% compared with the traditional technique such as resistance spot welding (RSW), due to the disadvantages of RSW, such as consuming electrode due to wear, high power consumption and high cost.

Friction stir spot welding (FSSW) is one of the advanced welding techniques which is derivative of friction stir welding (FSW). FSSW can be classified as a transient process due to its short cycle period. Both of FSW and FSSW use the same rotating tool [4]. The difference only between FSW and FSSW is that FSW has traverse movement, unlike FSSW. Unlike the fusion welding like TIG and MIG, the temperature during FSSW welding technique does not reach to the melting point of the parent metal, FSW run in the solid phase below the melting temperature of joining materials. The maximum temperature which was observed during FSW process between 0.6 T_m and 0.9 T_m [5]. Consequently, FSSW is classified as a solid-state welding technique, therefore hot cracking is excluded. FSSW is considered a "green technology", because of absence of consumable filler rods, shielding gas, environmental friendliness and energy efficiency [3]. The process of FSSW is mainly applied for lap joint as aluminum with aluminum, aluminum with steel or aluminum with magnesium.

There are many process parameters that determine the strength and the quality of the surface finish of the welded joint in FSSW such as rotational speed, geometry of the tool, dwell time, plunge depth, and the dimensions of the rotating tool [4].

High strength aluminum alloys such as 2xxx and 7xxx series have a critical problem where these alloys are difficult to be welded by conventional fusion welding such as TIG and MIG, therefore FSW is one of the successful welding processes which is used to weld these alloys with each other, and gives great results whether in mechanical properties or microstructure, due to many advantages such as: low distortion and residual stresses, no loss of alloying elements, no arc, no spattering, low noise, no fumes and free from porosity [6]. The improvements in the mechanical properties (i.e. yield strength and strain hardening rate) of the high strength aluminum alloys are produced because of the existence of the nanosized precipitates, which hinder the movement of dislocations.

The heat treatable aluminum 6xxx alloys have moderately high strength levels, better corrosion resistance than the 2xxx and 7xxx alloys, good weldability and higher extrudability [7]. The 6xxx series aluminum alloys are most commonly used for extrusion purpose and are widely used as vehicle body sheets. The 6xxx series alloys are heat-treatable and have the following advantages: good corrosion resistance, good surface finish, good formability, and medium strength. All these advantages make the 6xxx are suitable for structural applications. Magnesium and silicon are the main alloying elements in 6xxx aluminum alloys. These alloying elements are combined to form Mg₂Si compound, which makes the 6xxx alloys are heat treatable, and producing the medium strength. Although the AA6061 alloy can be joined by traditional fusion welding such as: TIG and MIG, the excess heat which occurred during these processes causing dissolution of its Mg₂Si compound which causing severe softening in the material and reduce the mechanical properties of the alloy [8].

Taguchi technique of Design of Experiments (DOE) is defined as an influential statistical method that permits optimizing the performance of a product, process, design and system with a significant reduction in the number of the experiments, time and costs [9]. Taguchi method is considered a special type of fractional factorial design. Taguchi determines the optimum conditions of parameters, which are unresponsive to the variation in environmental condition and other noise effects. There are three classes of quality characteristics defined in the analysis of signal to noise (S/N) ratio as the following: lower-the-better larger-the-better and nominal-the-best. The S/N ratio for each process parameter is calculated depending on S/N analysis function. A Larger S/N ratio is normally agreement with better quality characteristics regardless of the category. The level of larger S/N ratio is the optimal process parameter one. Analysis of variance (ANOVA) is performed to investigate which parameters have a significant effect on the quality characteristic [9].

From the previous studies, there are found many published studies on Friction Stir Welding and processing [10-13]. There are a few or absent information about using FSSW to weld similar aluminum alloys, especially using different designs for the anvil. The aim of this work is to study the effect of rotational speed, pin profile, penetration depth, design of the anvil on microstructure, and mechanical properties of these similar alloys joint, to achieve optimized properties, as much as possible.