



PREDICTION OF DUCTILE FRACTURE STRAINS IN UPSETTING PROCESSES

By Mostafa Khaled Megahed Ali Hassan

A Thesis Submitted to the Faculty of Engineering at Cairo University in Partial Fulfillment of the Requirements for the Degree of MASTER OF SCIENCE

in

Mechanical Design and Production Engineering

PREDICTION OF DUCTILE FRACTURE STRAINS IN UPSETTING PROCESSES

By Mostafa Khaled Megahed Ali Hassan

A Thesis Submitted to the
Faculty of Engineering at Cairo University
in Partial Fulfillment of the
Requirements for the Degree of
MASTER OF SCIENCE

in

Mechanical Design and Production Engineering

Under the Supervision of

Ass. Prof. Dr. Chahinaz Saleh

Department of Mechanical Design and Production Engineering Faculty of Engineering, Cairo University

Ass. Prof. Dr. Mostafa Shazly

Mechanical Engineering Department Faculty of Engineering, The British University in Egypt

FACULTY OF ENGINEERING, CAIRO UNIVERSITY GIZA, EGYPT 2020

PREDICTION OF DUCTILE FRACTURE STRAINS IN UPSETTING PROCESSES

By Mostafa Khaled Megahed Ali Hassan

A Thesis Submitted to the Faculty of Engineering at Cairo University in Partial Fulfillment of the Requirements for the Degree of

MASTER OF SCIENCE

in

Mechanical Design and Production Engineering

Approved by the Examining Committee	
Ass. Prof. Dr. Chahinaz A. R. Saleh,	Thesis Main Advisor
Ass. Prof. Dr. Mostafa Shazly	Advisor
Prof. Dr. Abdelrahman Ragab,	Internal Examiner
Prof. Dr. Mahmoud Mohamed M. Nemat-Alla, - Dean of the Faculty of Engineering, Kafr El-Sheikh	,

FACULTY OF ENGINEERING, CAIRO UNIVERSITY GIZA, EGYPT 2020 **Engineer's Name:** Mostafa Khaled Megahed Ali Hassan

Date of Birth: 14/2/1992 **Nationality:** Egyptian

E-mail: moustafakhaled14@gmail.com

Phone: +201115151580

Address: 41/14 St/El-shatr el-asher/New Maadi/Cairo

Registration Date: 1/10/2013 **Awarding Date:** .../.../2020

Degree: Master of Science

Department: Mechanical Design and Production Engineering

Supervisors:

Ass. Prof. Chahinaz Abdel Rahman Saleh

Ass. Prof. Mostafa Shazly

(Faculty of Engineering, The British University in Egypt)

Examiners:

Prof. Dr. Mahmoud Mohamed M. Nemat-Alla (External examiner)

(Dean of the Faculty of Engineering, Kafr El-Sheikh University)

Prof. Dr. Abdelrahman Ragab (Internal Examiner) Ass. Prof. Chahinaz A. R. Saleh (Thesis main Advisor)

Ass. Prof. Mostafa Shazly (Advisor)

Title of Thesis:

PREDICTION OF DUCTILE FRACTURE STRAINS IN UPSETTING PROCESSES

Key Words:

Ductile fracture; porous metal plasticity; finite element analysis, forming limit diagram at fracture, upsetting process.

Summary:

Forgeability and workability are measures of the plastic deformation limit that workpieces can undergo under bulk-forming processes. Upsetting tests for different axisymmetric specimens are usually used to construct the forming limit diagram at fracture (FLDF). The objective of the present work is to predict the FLDF for upsetting processes using coupled and Uncoupled DF approaches and relating the friction conditions and specimen dimensions to the critical height reduction of blocks. Numerical simulations are performed to determine the stress and strain distribution at the locations of crack formation. Two FE models are adopted after validating the results against published data; one considers voided materials while the other does not. It has been found that the coupled DF approach is in principle capable of predicting analytically the failure in upsetting processes. For uncoupled DF approach, an average value of the critical parameter (Cavg) in the out-of-plane shear and hydrostatic integrals has to be assigned from experiments to predict a semi empirically bilinear forming limit diagram at fracture FLDF. The fitting expression developed from the parametric study gives results close to the results obtained numerically with an error less than 9.69 %.



Disclaimer

I hereby declare that this thesis is my own original work and that no part of it has been submitted for a degree qualification at any other university or institute.

I further declare that I have appropriately acknowledged all sources used and have cited them in the references section.

Name: Mostafa Khaled Megahed Ali Hassan Date: .../.../2020

Signature:

Dedication

I dedicate this work to all interested and knowledge eager folks.

Acknowledgments

I would like to thank all the people who contributed in some way to the work described in this thesis. First, I thank my academic advisor, Dr. Chahinaz for her time, effort and patience.

I would like to thank my family who supported me through these years. I would like to thank my wife Fatma for her constant love, my mom for her prayers and my father for his support.

Table of Contents

DISCLAIMER		I
DEDICATION		II
ACKNOWLED	OGMENTS	III
TABLE OF CO	ONTENTS	IV
LIST OF TABI	LES	VI
LIST OF FIGU	JRES	VII
NOMENCLAT	CURE	X
LIST OF ABBI	REVIATIONS	XII
ABSTRACT		XIII
CHAPTER 1:	INTRODUCTION	1
CHAPTER 2:	LITERATURE REVIEW	3
2.1. 2.1.1. 2.1.2. 2.2. 2.2.1. 2.2.2. 2.3. 2.3.1. 2.3.2. 2.3.2.1 2.3.2.2 2.4. 2.5.	2. Uncoupled approach SCOPE OF WORK. THESIS STRUCTURE	lity3 ality81014 E FLDF IN1516 Diagram at181820
CHAPTER 3:	THEORETICAL BACKGROUND	23
3.1. 3.2.	REVIEW OF CONSTITUTIVE RELATIONS USED FOR COUPLEI FRACTURE ANALYSIS REVIEW OF EQUATIONS FOR UNCOUPLED DUCTILE ANALYSIS	23 Fracture
CHAPTER 4:	FEA OF UPSETTING PROCESSES: CHARACTERIST	ICS AND
VALIDATION		- 1

4.2. 4.3.	
1 2	DYNAMIC EXPLICIT ANALYSIS IN ABAQUS
4.3.	SPECIMENS' GEOMETRIES
4.4.	THE AXISYMMETRIC FINITE ELEMENT MODEL
4.4.1.	Axisymmetric model validation36
4.4.2.	Comparison with Dadras [94](semi-empirical) model4
4.5.	THREE-DIMENSIONAL FINITE ELEMENT MODEL
4.5.1.	Validation of the rectangular block model45
4.6.	MECHANICS OF DEFORMATION OF BILLETS UNDER THE UPSETTING PROCESS
4.6.1.	Effect of friction conditions, specimen configuration and type o material
4.6.2.	Stress triaxiality range in the upsetting process and its effect on the crack shape
	PREDICTION OF FORMING LIMIT DIAGRAM AT DF59
	DETERMINATION OF FORMING LIMIT DIAGRAMS AT FRACTURE (FLDF
ACTURE FL 5.1.	DETERMINATION OF FORMING LIMIT DIAGRAMS AT FRACTURE (FLDF USING A COUPLED APPROACH
5.1. 5.1.1.	DETERMINATION OF FORMING LIMIT DIAGRAMS AT FRACTURE (FLDF USING A COUPLED APPROACH
5.1. 5.1.1. 5.1.2.	DETERMINATION OF FORMING LIMIT DIAGRAMS AT FRACTURE (FLDF USING A COUPLED APPROACH
ACTURE FL 5.1. 5.1.1.	DETERMINATION OF FORMING LIMIT DIAGRAMS AT FRACTURE (FLDF USING A COUPLED APPROACH
5.1. 5.1.1. 5.1.2.	DETERMINATION OF FORMING LIMIT DIAGRAMS AT FRACTURE (FLDF USING A COUPLED APPROACH
5.1. 5.1.1. 5.1.2. 5.2.	DETERMINATION OF FORMING LIMIT DIAGRAMS AT FRACTURE (FLDF USING A COUPLED APPROACH

List of Tables

Table 2.1: Review of coalescence criteria from literature (with modification) [23]	13
Table 2.2: Uncoupled models with two constants or more [5]	15
Table 4.1: Geometry utilized in validation of FEA and designation of the equator.	(All
dimensions are in mm).	32
Table 4.2: Data of published upsetting models used in the axisymmetric validation.	37
Table 4.3: Stress triaxiality range and failure strain for different upsetting configurate	tions
made of different materials with shown crack orientation	56
Table 5.1: Material parameters and experimental plane strains values at failure	for
different specimen configurations.	64
Table 5.2: Values of Cave of both materials regarding the failure mechanism	73
Table 5.3: FE models used in the analysis (all dimensions in mm)	74
Table 5.4: Trials used in deducing a parametric experssions	76

List of Figures

Figure 1.1: Ductile fracture: a) cylindrical upsetting [6], b) Extrusion[7]
Figure 2.1: Void nucleation by Matrix-particle decohesion (a) or particle cracking (b) [24].
Figure 2.2: Void nucleation in shear bands initiated at ferrite cementite interface in pearlitic steel [25]
Figure 2.3: Voids growth with rotation and shape change at shearing incipient of a copper alloy [3], [36]6
Figure 2.4: Internal necking in the middle region of the necked section of an as-rolled copper tensile specimen [29]6
Figure 2.5: Void linkage by void sheeting in AISI 4340 steel at a plastic strain equal to 0.25 [28]
Figure 2.6: Coalescence by necking and simple touching of voids in low alloy steel [37]7
Figure 2.7: Void coalescence under high positive stress-triaxiality (a) and under low positive stress-triaxiality (b) [13]
Figure 2.8: Fracture surface photographs of A12024-T351 under upsetting of cylindrical specimens [5]9
Figure 2.9: cross-section in the fracture surface through the matrix material [5]9 Figure 2.10: Different fracture strains of cold-drawn 1045 steel at the equatorial surface in different cylindrical upsetting processes [88]
and line 2 represents mode I) [91]
Figure 2.13: Silva's forming limit covering stress triaxiality from -0.2 to 0.6 (c stands for cylindrical specimens, t for tapered and f for flanged), Mode I (opening) and Mode III (shearing) [95]
Figure 3.1: Fracture modes in upsetting (a) shearing mode, (b) opening mode29 Figure 4.1: Quarter cylindrical portion used in FEA33
Figure 4.2: Details of the axisymmetric model
Figure 4.4: Variation of the equivalent plastic strain at the equatorial surface for different mesh sizes
Figure 4.5: Mesh size grading from bigger to smaller
Figure 4.7: Comparison of the strain path for a point at the equatorial as predicted by the present model and the experimental results of [83]
cylinderical upsetting tests at coefficient of friction equal to 0.1 . (a) $H/D = 1$ [C2]. (b) $H/D = 1.5$ [C3]. (see Table 4.2)
Figure 4.9: Variation of the diameteral change ΔD with the axial displacement U as predicted by the FE model and the experiment of Radić [104]40

Figure 4.10: Variation of the ratio between hydrostatic stress and equivalent matrix stress
with respect to axial strain for the current FE model and Dadras model [94]41
Figure 4.11: Variation of the ratio between Axial stress and equivalent matrix stress with
respect to Axial strain for the current FE model and Dadras model [94]42
Figure 4.12: Variation of the ratio between tangential stress and equivalent matrix stress
with respect to axial strain for the current FE model and Dadras model [94]42
Figure 4.13: Eighth of the specimen used in FEA44
Figure 4.14: Specimen description with its symmetry planes44
Figure 4.15: Flow stress-strain relation for commercially-pure aluminum used in FE
model [105]
Figure 4.16: Deformed symmetry planes at 40 % HR as shown in x-z plane (a) and in x-
y plane (b)
Figure 4.17: Comparison between the experimentally detected deformed billet profile
and the FE results of Pillinger et al. [105] and the present model at 40 % reduction47
Figure 4.18: Comparison between the experimental and predicted forging load for Initial
heights (H ₀) of 5.25 mm and 7.65 mm at frictionless condition
Figure 4.19: Variation of normalized plane stresses $\sigma\theta$, σZ through upsetting process for
cylindrical speciemen made of AISI 1040 for different contact conditions. (H/D = 1.125).
Figure 4.20: Variation of normalized axial stress σZ for two different material AISI 1040
and AL2024-T351 (H/D=1.125 and m=0.2)50
Figure 4.21: Strain path of two different material AISI 1040 [82] and AL2024-T351 [5]
at 1.125 aspect ratio with different friction conditions
Figure 4.22: Variation of the normalized plane stresses $\sigma\theta$, σZ through upsetting of AISI
1040 cylindrical specimen with different aspect ratios at m=0.3
Figure 4.23: Strain path of AISI 1040 [82] for different aspect ratios at m=0.3
Figure 4.24: Variation of the normalized plane stresses $\sigma\theta$, σZ through upsetting of AISI
1040[82] axisymmetric specimens with different configurations.
Figure 4.25: Strain path of AISI 1040 [82] for different axisymmetric configuration53
Figure 4.26: Vertical strain distribution and deformed shape for tapered and flanged
compression specimens at H.R. 61.3 % and with $\mu = 0.15$
Figure 4.27: Two failure modes shown for AA2030-T4 flanged upsetted specimen,
(mode I) "opening" conventional DF mode and (mode III) "shearing" [95]57
Figure 5.1: Coalescence point determination for a cylindrical specimen (C1) of AISI
1040 steel with and without shear effect, at $CVo = 0.01$ and $\lambda 1i = \lambda 2i = 0.2$ 60
Figure 5.2: Forming limit curves for AISI 1040 of different initial void volume fraction
CVo (n = 0.226, $\lambda 1i = 1$) according to McClintock condition [2], [3], [11]61
Figure 5.3: Forming limit curves for different strain-hardening exponents n (CVo=
$0.02, \lambda 1i = 1$) according to McClintock condition [2], [3], [11]62
Figure 5.4: Forming limit curves for different Initial void shapes $\lambda 1i$ (CVo=
0.02, n = 0.226) according to McClintock condition [2], [3], [11]63
Figure 5.5: Comparison between the predicted limit curves FLDF using different criteria
with experimental failure points for AISI 1040 steel. Shear Effect are not considered in
void shape evolution65
Figure 5.6: Comparison between the predicted limit curves FLDF and the experimental
failure points for AISI 1040 steel. The effect of shear on void shape evolution are
considered66
Figure 5.7: Comparison of predicted limit curves FLDF with experimental failure points
for AISI 1045 steel. The predicted bounding limit curves corresponds to initial void
volume fraction range without adding the shear effect

Figure 5.8: Comparison of predicted limit curves FLDF with experimental failure points
for AISI 1045 steel with applying the shear condition
Figure 5.9: Comparison of predicted limit curves FLDF at $\lambda 1i = 0.2$ according to Ragab
[10] criteria with CVo= 0.0001 and McClintock [2], [3], [11] with CVo= 0.02 with
experimental failure points of AISI 1040 steel69
Figure 5.10: Critical values for the damage parameter C estimated according to two
failure modes for the different specimen configurations, (a) AISI 1040 and (b) AISI 104571
Figure 5.11: Bilinear fracture limit for AISI 1040 and AISI 1045 steels compared to the
theoretical limit of Kuhn et al. [88]72
Figure 5.12: Bilinear fracture limit for AISI 1045 compared with experimental failure
points of Kuhn et al. [88]73
Figure 5.12: Billet dimensions used in the analysis

Nomenclature

 C_{v_o} , C_v Initial and current Void volume fraction Tvergaard adjusting parameters q_1, q_2, q_3 \mathbf{C} Critical damaged parameter of uncoupled integrals $\bar{\varepsilon}$ Equivalent strain Effective strain for the matrix $\overline{\epsilon}_e$ Equivalent elastic strain $\overline{\epsilon}_e$ Equivalent plastic strain $\overline{\epsilon}_p$ $ar{arepsilon_f}$ Equivalent strain at failure ϵ_{v}^{p} Volumetric plastic strain Principal strains from maximum to minimum $\varepsilon_{1,2,3}$ Tangential and axial strain $\varepsilon_{\theta}, \varepsilon_{z}$ Stress terms in the stress tensor σ_{ij} Hydro static stress σ_m $\overline{\sigma}$ Macroscopic von-Mises flow stress Equivalent stress for the matrix $\bar{\sigma}_{M}$ Principal stresses from maximum to minimum $\sigma_{1,2,3}$ Tangential and axial stress σ_{θ} , σ_{z} C^e Elasticity matrix λ Plastic multiplier λ_{1i}, λ_1 Initial and current void aspect ratio λ_{2i}, λ_2 Initial and current unit cell aspect ratio $\frac{b_1}{b_2}$ Ligament size ratio Strain hardening exponent n D Shear damage Lode angle dependence function g_{θ} θ_{l} Lode angle Out of plane shear stress τ_{13} Coefficient of friction μ Е Modulus of elasticity

υ Poisson's ratio

H/D Height to diameter ratio